

GEOTECHNICAL AND GEO-ENVIRONMENTAL ASSESSMENT

**Client: West Somerset and Taunton Deane
Borough Council**

Watchet Harbour East Quay

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SOUTH WEST GEOTECHNICAL

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Executive Summary

South West Geotechnical Ltd (SWG) was commissioned by Pick Everard, on behalf of West Somerset and Taunton Deane Borough Council (the Client) to undertake a geotechnical and basic geo-environmental assessment of the East Quay at Watchet Harbour, West Somerset.

The purpose of the investigation works was to determine the ground conditions on site and to undertake stability analysis of the global stability of the quay wall.

Desk Study

The bedrock geology comprises a combination of the Mercia Mudstone Group (MMG) and the Blue Lias Formation (BLF).

An investigation was undertaken by Parkman Environment at the site in 1997. The investigation encountered made ground to depths of between 2.3 and 6.2m with the upper level of the MMG and BLF bedrock below these depths.

Ground Conditions

The investigation encountered made ground overlying the upper surface of the MMG and BLF bedrock. BHs 101, 102 and 103 encountered MMG materials whilst BHs 104 and 105 encountered BLF. Noticeably poorer ground conditions were encountered at depth in BH103 suggesting the faulted contact between the two geological units is in close proximity to this borehole.

Tidally influenced groundwater conditions are present.

Geo-environmental

The ground investigation and subsequent laboratory testing indicated have confirmed low contaminant concentrations and no remediation is required with regards to contaminated soils.

The materials are likely to be classed as non-hazardous from a waste perspective.

Geotechnical and Geo-environmental Assessment

Should any obviously contaminated soils be encountered during the construction phase of the works, advice should be sought from a suitably experienced Geo-environmental Engineer.

Geotechnical

The stability analysis indicates that the stability of the wall in its current state is marginal. It is evident from investigations into the wall that it is narrow and has not been adequately designed to modern standards. This is not uncommon of historic quay walls in the south west.

It is considered that replacing the existing structure with a new, appropriately designed wall / crane supporting structure is necessary.

Three potential options could be considered for construction of a new wall in front of the existing structure as follows:

- Sheet piled wall.
- Construction of solid masonry retaining structure.
- Bored Pile Wall/ Crane Deck.

It is likely that further investigation, including rotary boreholes, will be required to enable an economic piled foundation design.

The Mercia Mudstone and Blue Lias bedrock at the base of the existing wall will provide adequate support to either gravity or piled foundations.

1 INTRODUCTION

1.1 General

South West Geotechnical Ltd (SWG) was commissioned by Pick Everard, on behalf of West Somerset and Taunton Deane Borough Council (the Client) to undertake a geotechnical and basic geo-environmental assessment of the East Quay at Watchet Harbour, West Somerset.

Pick Everard are the Structural Engineers for the project. The scope of works is broadly based on Pick Everards Scope of Works for Geotechnical Consultants (JRB/MGA/180968/10-11/2685-PEV-XX-XX-RP-S-0001- Issue No P01, dated 31.07.18).

1.2 Aims

The quay is currently used for boatyard operations, including the lifting of boats in and out of the harbour by crawler and mobile cranes. It is understood the change are to be made to the operation of the quay, including the use of a new crawler crane. To enable an assessment of the quay wall stability a ground investigation was required to determine the strength and nature of the soils and rock behind and beneath the quay wall. As part of the over stability assessment, SWG undertook an assessment of the potential for a slip failure beneath the wall.

1.3 Site Description

The site comprises a 10m strip along the edge of the east quay at Watchet Harbour. The site is roughly level and largely concrete surfaced. The northern third of the quay is surfaced in a mixture of tarmac and patches of poorer quality concrete.

The quay wall is essentially split into three sections, northern, central and southern. The northern and southern sections are constructed of stone blocks and these represent the original wall construction. The central section of the wall comprises a series of sheet piles with ground anchors. It is understood this section of the wall was constructed following a major collapse of the wall.

Geotechnical and Geo-environmental Assessment

From a diver survey of the quay wall (undertaken by others), it is understood that the height of the quay wall to the silt within the harbour is between 6.60m and 6.90m, and between 8.45m and 9.90m to the bed rock.

Three shipping containers, converted for use as art studios and an art gallery, were located at the southern end of the quay.

The site location plan is included in Appendix A.

2 DESK STUDY

2.1 Geology

The site is located in a geologically complex area. The complexity is shown on the Envirocheck geology map included in Appendix B.

The bedrock geology comprises a combination of the Mercia Mudstone Group (MMG) and the Blue Lias Formation (BLF).

The MMG comprises weakly cemented interbedded mudstone, siltstone and sandstone grade materials. The materials are generally “massive” with widely spaced discontinuities. It is common for these rocks to be deeply weathered near surface and altered to predominantly cohesive soils although given the sites coastal location, any soils are expected to have been eroded. Evaporitic minerals containing sulphates (gypsum and halite) are known to occur within the MMG series of rocks.

The BLF comprises interbedded mudstone, siltstone and limestone. The mudstone and siltstone grade materials are typically extremely weak to very weak with the limestone being medium strong. The bedding of the materials is generally close to medium spaced as evidenced by outcrops on the beach to the north of the site.

The area is intensely folded and faulted as shown on the geology map and on freely available aerial photography. Faults are a result of brittle deformation of the bedrock and rock in the vicinity of faults typically have poorer engineering properties than un-faulted rocks. Faults also act as a conduit for groundwater flow. An east-west striking fault is shown to be present cutting through the southern part of the harbour.

The British Geological Survey Map for the area (Sheet 278, Minehead) shows the dip of the primary discontinuity set of the bedrock (Bedding) in the area to have highly variable angles and orientations. This highlights the highly complex nature of the structural geology of the area.

2.2 Previous Investigations

An investigation was undertaken by Parkman Environment at the site in 1997. The investigation comprised seven trial pits and four boreholes.

The boreholes were undertaken using cable percussive techniques. These are soft ground boring techniques and so limited data is available on geotechnical parameters for the bedrock beyond Standard Penetration Tests (SPTs).

The investigation encountered made ground to depths of between 2.3 and 6.2m with the upper level of the MMG and BLF bedrock below these depths.

The made ground was a combination of cohesive and granular soils which are largely reworked local soils with fill materials. Locally railway ballast and clinker materials were present.

The MMG was encountered as very stiff consistency clay with mudstone gravel.

3 GROUND INVESTIGATION

3.1 Fieldwork

An intrusive investigation was carried out between 6 and 16 November 2018, comprising the following:

- 2 no UKAS accredited plate load tests
- 5 no multi-technique boreholes
- Groundwater monitoring

The fieldwork was carried out following the guidelines of BS 5930 (2015): Code of Practice for Ground Investigation; British Standard BS10175 (2011): Investigation of Potentially Contaminated Sites – Code of Practice and BS EN 1997-2:2007 (Eurocode 7) – Geotechnical Design – Part 2: Ground investigation and testing).

The exploratory were positioned approximately at the locations selected by the Engineers for the project (Pick Everard). Locations of the exploratory holes are shown on the Exploratory Hole Location Plan, enclosed as Appendix C.

3.2 Multi-technique Boreholes

Five (5 No) boreholes were undertaken by a combination of techniques on the site using a Comacchio Geo205 multi-purpose rig.

Boreholes were advanced through soils using dynamic sampling with in-situ Standard Penetration Tests (SPTs) down to rock head, followed by rotary coring to enable approximately 5.0m of rock core to be recovered.

Where SPT blow counts exceed 50 without the reaching the full 300mm penetration, the actual penetration was recorded and the extrapolated N-value for the full penetration was calculated and plotted.

The coring was undertaken using an air-mist flush. Core samples were recovered from the core barrel in plastic liner and placed in wooden core boxes prior to being logged by a Geotechnical Engineer.

3.3 Plate Load Tests

Two UKAS accredited Plate Load Tests were undertaken on the site at locations agreed with the Engineer. PL01 was undertaken behind the central section of the quay wall and PL02 was undertaken behind the northern section of the wall. Both tests were undertaken at a depth of 0.20m following removal of the concrete surface/slab. The tests were undertaken to a maximum applied pressure of 208 kPa, in accordance with the Engineers requirements.

Plate Load Test Results are included in Appendix E.

3.4 Groundwater Monitoring Standpipes

Groundwater monitoring standpipes were installed in the boreholes to facilitate groundwater monitoring. The standpipes comprise a 50mm diameter slotted pipe with gravel cell from the base of the hole to near surface and plain pipe with bentonite seal to ground level, finished with a flush cover at ground level.

Electronic level loggers were installed in the boreholes to enable accurate groundwater data to be collected, in particular to measure any tidal influence.

4 LABORATORY TESTING

4.1 Geotechnical Laboratory Testing

All geotechnical testing was carried out in the SWG UKAS accredited laboratory in accordance with BS 1377; 1990, Methods of tests for soils for civil engineering purposes. Table 1 summarises geotechnical testing undertaken. The geotechnical laboratory test results are enclosed as Appendix F.

Table 1: Geotechnical Testing

Test	No. Tests
Soil	
Moisture Content	9
Atterberg Limits	9
Particle Size Distribution Sieve	7
Shear Box	1
pH & Soluble Sulphate	10
Rock	
Point Load Test	10
Uniaxial Compressive Strength Test	4

4.2 Geo-environmental testing

The investigation was not intended to be a full geo-environmental audit. However, a number of samples were obtained and tested for the suite of contaminants detailed in Table 2. The geo-environmental laboratory test results are enclosed as Appendix G.

Table 2: Geo-environmental Testing

Test	No. Tests
pH, Organic Matter, Sulphate (water soluble)	5
Speciated Polyaromatic Hydrocarbons (PAH)	5
Speciated Total Petroleum Hydrocarbons (aliphatic / aromatic split)	5
Asbestos screen	5
BTEX	5

Two Waste Acceptance Criteria (WAC) leachate analysis tests were undertaken on made ground materials.

5 GROUND CONDITIONS

5.1 Strata Encountered

The investigation encountered made ground overlying the upper surface of the MMG and BLF bedrock. BHs 101, 102 and 103 encountered MMG materials whilst BHs 104 and 105 encountered BLF. Noticeably poorer ground conditions were encountered at depth in BH103 suggesting the faulted contact between the two geological units is in close proximity to this borehole. The strata encountered in each borehole is summarised in Table 3.

Table 3: Stratum Summary

Stratum	BH ID and Maximum Depth of Stratum (m bgl)				
	BH101	BH102	BH103	BH104	BH105
Made Ground	6.0	6.2	7.2	6.5	5.2
Mercia Mudstone	>12.5	>12.5	>12.5		
Blue Lias				>12.4	>10.5

Standard Penetration Tests (SPTs) were undertaken at frequent intervals in the dynamic sample sections of the borehole to allow the relative strength / density of near surface soils to be assessed. The SPT N values have been plotted against depth in Figure 1.

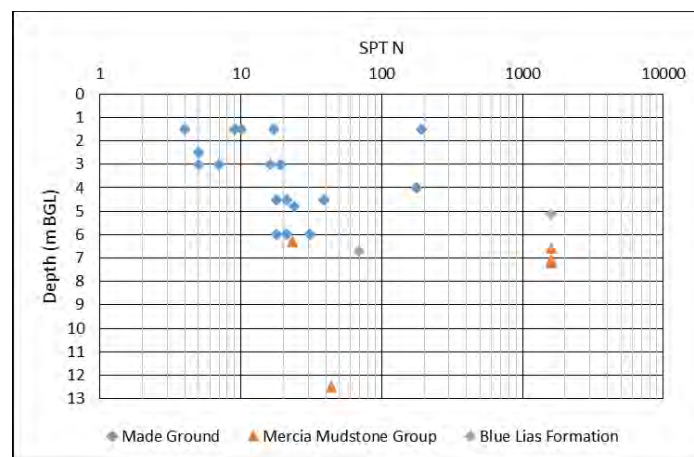


Figure 1: SPT N Vs Depth Plot

5.2 Made Ground

Surface coverings of tarmac or concrete were encountered in each exploratory hole. The concrete was 0.2m thick and contained 6mm diameter steel reinforcement.

Made ground extends to depths of between 5.2 and 7.2m below ground level. The heterogeneous materials are both cohesive and granular in nature and comprise essentially reworked local soils with fill materials including limestone boulders ash and clinker.

The cohesive made ground materials are generally very soft to soft consistency, sandy, gravelly clay. Locally the materials are firm and stiff consistency.

The more granular materials comprise loose to dense clayey gravel.

SPT N values recorded in the materials range from 4 to 192 (extrapolated). The high values ($N > 50$) are coincident with boulders (BH101) and possibly sections of old wall (BH105). Discounting the high values, the average SPT N value for the materials is 16.

Liquid and Plastic (Atterberg) Limit tests undertaken on the cohesive made ground materials indicate the soils have low to intermediate plasticity (CL/CI).

Particle Size Distribution Sieves undertaken on the more granular made ground indicates the majority of the materials are gravel with relatively low fines content (Figure 2). More cohesive soils such as BH103 (2.8m) have a high sand content.

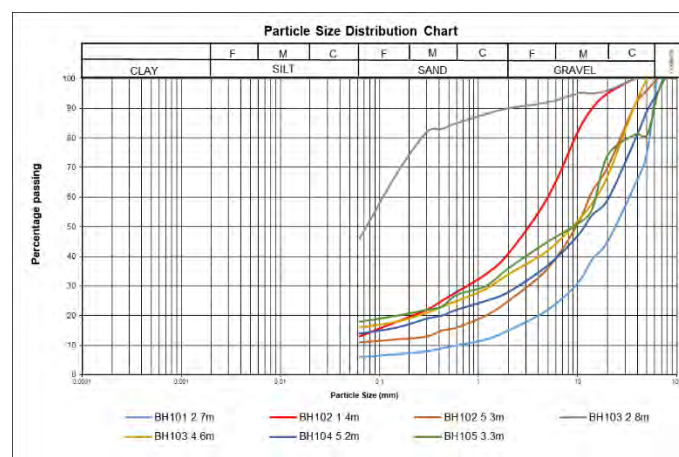


Figure 2: Particle Size Distribution Summary

A single shear box was undertaken on more granular made ground materials. This gave a friction angle of 34° for the soils.

Using correlations between plasticity and friction angle gives a basic friction angle of 28° for the more cohesive made ground.

5.3 Mercia Mudstone Group

The Mercia Mudstone Group materials were encountered in BHs 101, 102 and 103 undertaken along the more northern section of wall at depths of between 6.0 and 7.2m below ground level.

The materials generally comprise very weak to weak, closely to medium fractured mudstone. In general Rock Quality Designation (RQD) values are high (typically $>40\%$) although towards the base of BH103, the RQD values are 0% and coincide with much lower strength (extremely weak) material. The low RQD and corresponding extremely weak rock is potentially indicative of the faulted contact between the MMG and BLF.

Laboratory strength tests undertaken on the MMG materials are summarised in Figure 3. The UCS test values (normalised) and UCS values derived from Point Load Tests confirm the range of strengths of the MMG materials with values ranging from 0.9 to 22 MPa.

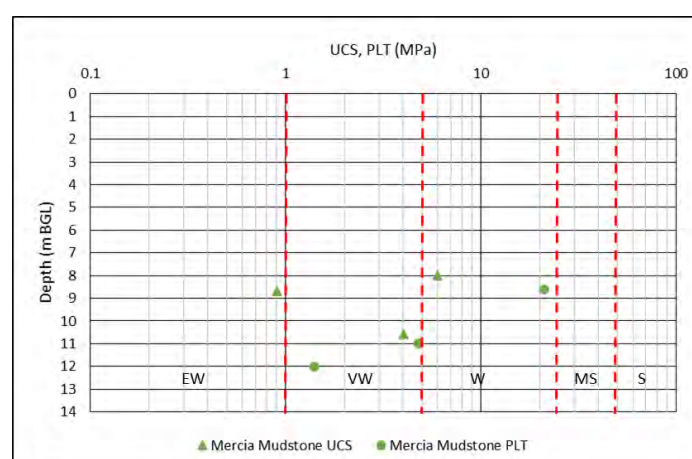


Figure 3: Laboratory Strength Test Results MMG

In order for parameters of cohesion and friction to be derived for the MMG rock mass, Geological Strength Index (GSI, Hoek and Marinos 2000) values have been determined for

the materials using the logging and laboratory strength data. Figure 4 summarises the GSI values determined for the MMG per metre of core. The average GSI value is 46 with the lower value (34) corresponding with the potentially faulted materials in BH103.

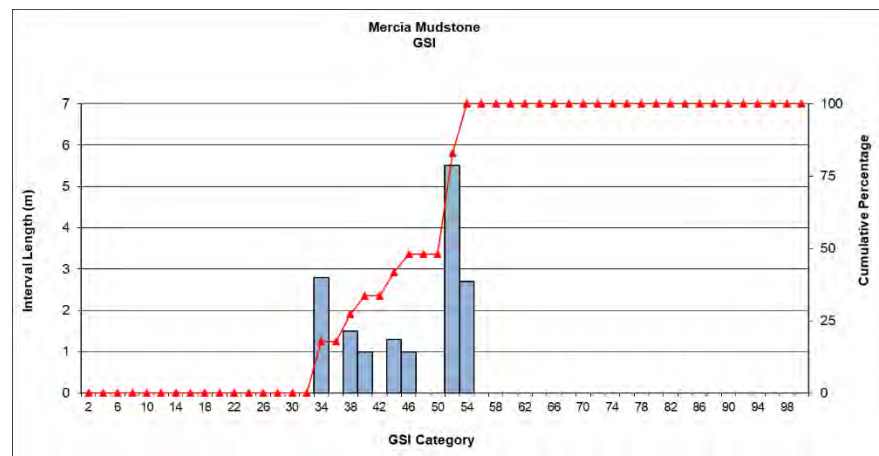


Figure 4: Histogram of GSI intervals for MMG

5.4 Blue Lias Formation

The Blue Lias Formation materials were encountered in BHs 104 and 105 undertaken along the more southern section of wall at depths of between 5.2 and 6.5m below ground level.

The materials generally comprise very weak and weak, closely to medium fractured mudstone. A band of strong limestone was encountered between 7.5 and 7.9m in BH105. The Rock Quality Designation (RQD) values are high (>50%).

The dip of the primary discontinuity set (bedding) in the materials is approximately 30-40°. The orientation of the bedding (dip direction) is not known although it is potentially to the north on the basis of the geology map.

Laboratory strength tests undertaken on the BLF materials are summarised in Figure 5. The UCS test values (normalised and UCS values derived from Point Load Tests confirm the range of strengths of the BLF materials with values ranging from 11 to 68 MPa. The high value (68 MPa) is representative of the limestone.

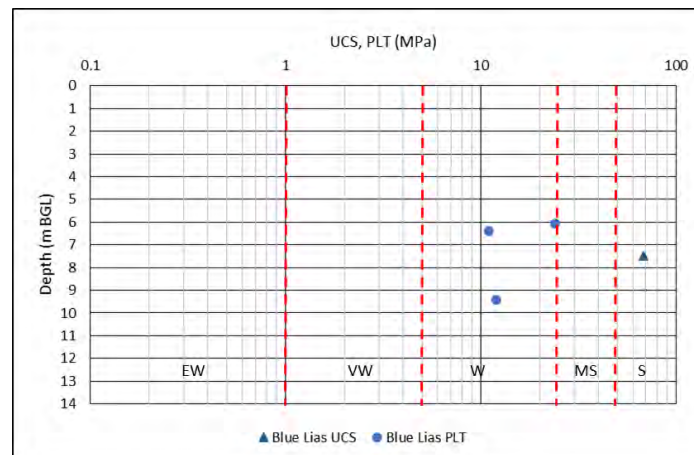


Figure 5: Laboratory Strength Test Results BLF

Geological Strength Index (GSI, Hoek and Marinos 2000) values have been determined for the materials using the logging and laboratory strength data. Figure 6 summarises the GSI values determined for the BLF per metre of core. The average GSI value is 48 with the high value (65) corresponding with the limestone.

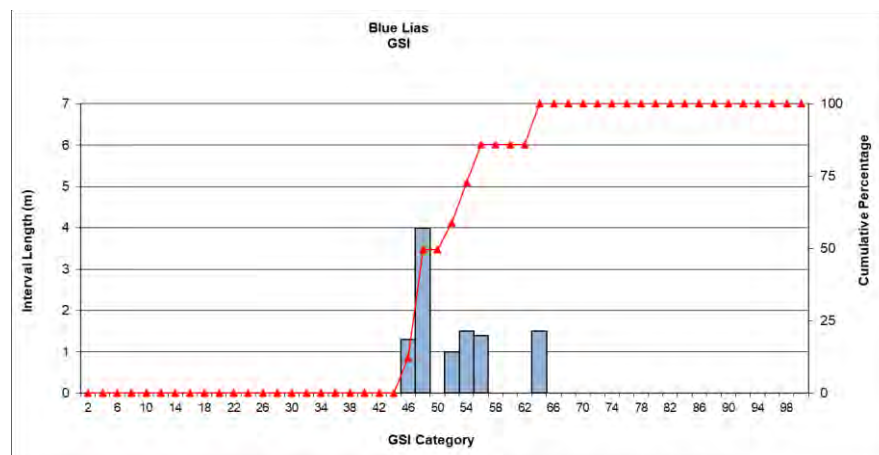


Figure 6: Histogram of GSI intervals for BLF

5.5 Groundwater

Barometric Level loggers were installed in all five boreholes between 17 November and 3 December 2018 to enable the groundwater levels to be monitored. The data is summarised in Figure 7. It is evident that the water levels in BHs 101, 102 and 103 are heavily tidally influenced with fluctuations mirroring tidal movements.

The tidal influence on boreholes 104 and 105 is much less pronounced, possibly due to the rock head levels being higher in BHs 104 and 105.

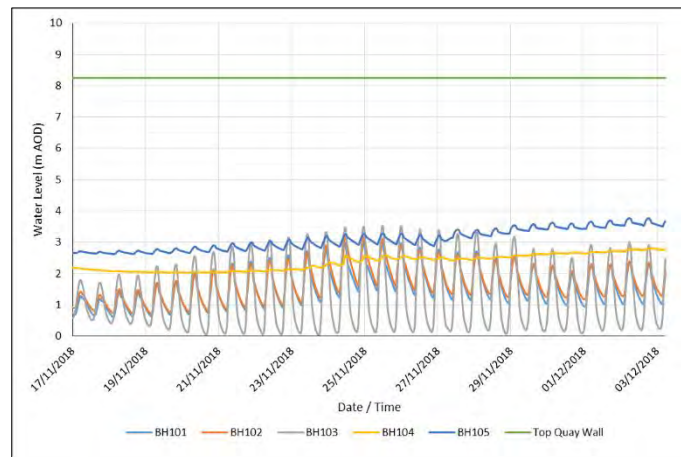


Figure 7: Barometric Logger Groundwater Level Summary

5.6 Signs of Contamination

In general, no visual or olfactory evidence of significantly contaminated soils was noted in the exploratory holes. However, ash and clinker material were encountered in BH102 and BH104.

6 GEO-ENVIRONMENTAL ASSESSMENT

6.1 General

The investigation was not intended to be a full geo-environmental audit. Instead, samples were collected primarily for construction worker health and safety and waste disposal purposes.

The contamination assessment has been carried out following the guidelines outlined in the Chartered Institute of Environmental Health (CIEH) & Contaminated Land: Applications in Real Environments (CL:AIRE) document – Guidance on Comparing Soil Contamination Data with a Critical Concentration, May 2008 and Environment Agency (EA) documents: SR2, SR3, SR4, SR7 & CLR11 using a source-pathway-receptor analysis method, so that an appropriate conceptual model can be developed.

On the basis of the desk study information and walkover survey, although some potential sources of contamination were identified, extensive contamination was not expected to be present.

6.2 Geo-environmental Soil Test Results

The results of the environmental laboratory testing, presented as Appendix G, have been compared to Suitable for Use Level (S4UL) values for commercial/industrial developments. For organic substances a 1% Soil Organic Matter (SOM) has been used, unless otherwise indicated, which represent the most stringent threshold limit.

LQM/ CIEH S4ULs have been developed by Land Quality Management Ltd jointly with the Chartered Institute of Environmental Health, and provide values for the assessment of potential risks to human health posed by contaminants in soil, and are compliant with UK legislative policy and guidelines. In particular, these include components of TPH and PAH. The S4ULs have been derived in accordance with UK legislation, national as well as Environment Agency (EA) policy, and using a modified version of the EA CLEA software. The Department for the Environment, Food & Rural Affairs (DEFRA) has published Category 4 Screening Levels (C4SLs) for six substances including lead. The C4SLs represent the most stringent guidance available for the assessment of lead contamination in soils, and have been used in this report.

Where other guidelines are not available, local guidance, Dutch standards or an in-house screening value is used to provide an initial comparison figure.

Very low contaminant levels were recorded across the site, with all recorded concentrations well below the relevant guideline values for commercial/ industrial use. Indeed, recorded hydrocarbon (TPH and PAH) concentrations are generally below detection limits.

No asbestos fibres or ACM fragments were recorded in the samples tested.

6.3 Human Health (Soils) Risk Assessment

In order for land affected by contamination to cause harm, there must be a source of contamination, a receptor that can be harmed and a pathway by which the receptor can be exposed to the contamination.

Based on the very low recorded contamination concentrations there is effectively no source and therefore no significant risk to possible receptors (future site users, construction works and the wider environment). Furthermore, as the site like to remain or be almost entirely hard covered, the risk to receptors is even further reduced.

6.4 Waste Acceptance Classification

The geo-environmental testing did not indicate any significantly elevated contaminants. The two WAC tests undertaken indicate the made ground soils exceed the limits for inert waste in the basis of elevated antimony and sulphate (BH102) and chloride (BH104). Therefore it is likely that the materials would be classified as non-hazardous in term of waste classification.

The results of the testing should be forwarded to preferred landfill operators who will determine the classification of the materials.

6.5 Remediation Requirements

The ground investigation and subsequent laboratory testing indicated have confirmed low contaminant concentrations and no remediation is required with regards to contaminated soils.

Geotechnical and Geo-environmental Assessment

Should any obviously contaminated soils be encountered during the construction phase of the works, advice should be sought from a suitably experienced Geo-environmental Engineer.

7 GEOTECHNICAL ASSESSMENT

7.1 General

The investigation has highlighted that the made ground materials behind the wall predominantly comprise reworked local soils which are highly variable in terms of consistency (heterogeneous) with very low and low strength cohesive soils and locally loose granular soils present.

The SPTs and laboratory test results suggest the soils have variable and poor drained strength parameters (cohesion and friction).

The investigations focusing on quay wall construction (undertaken by others) indicate the wall is also highly variable. At the northern end (BHs 101 and 102), the wall is approximately 1.2-1.3m thick mass concrete. Through the central section (BH103) it is understood the sheet piles have horizontal tie-bars adding support. At the southern end in the vicinity of BH104 and 105, the wall is thin (0.6m) approx. masonry face potentially with soft clay behind.

It is evident that sections of the wall have failed in the past and have been rebuilt on an ad-hoc basis to ensure the serviceability of the harbour.

Proposals involve utilising large cranes on the site in a 10m wide corridor at the top of the quay wall. It is understood the cranes have the potential to generate very high point loads of up to 830 kN/m².

7.2 Initial Stability Assessment

In order to assist with determining the overall stability of the quay wall, two cross sections have been constructed through the wall based on sections provided in the Pick Everard presentation document JRBB/MGA/180968/17-2/R005 - Issue Number 01 and the findings of the ground investigation. These sections are through the northern and southern sections of the quay wall.

The initial stability of the area has been assessed using limit equilibrium (LE) stability analysis, undertaken using Rocscience SLIDETM slope stability software.

When discussing stability using LE methods, the analysis is undertaken by determining a Factor of Safety (FoS) for the section in terms of the resisting forces preventing movement and driving forces causing movement. When the driving forces exceed the resisting theoretical failure occurs. A section with a FoS of 1.0 is in equilibrium and therefore in a state of marginal stability.

It should be noted that due to the complex overturning moments involved in retaining walls failing, LE methods of analysis do not allow accurate modelling of the failure mechanisms (i.e. failure due to overturning). However, when a retaining wall is considered as a block, the LE analysis can provide an indication of whether the retaining wall is “robust” enough (i.e. thick enough to resist the disturbing forces acting through the soil behind it).

The method does not consider the three dimensional effect of buttressing such as that acting on the northern and southern extremities of the wall (i.e. where the wall changes direction around the harbour).

It has not been possible to assess potential failure through the central sheet piled section of the quay wall, as this section is anchored back and we have no information as to how much ‘work’ (added strength) the anchors are doing and this will be crucial to the stability analysis.

On the basis of the above, the analysis is not considered a comprehensive stability assessment of the wall but it does provide important indicators of the potential stability and external forces acting to increase/ decrease the stability of the wall.

7.2.1 Stability Analysis Method

Analysis was undertaken using the GLE/Morgenstern & Price method and follows traditional British Standard methods where by a FoS of 1.0 indicates equilibrium rather than Eurocode methods where factors are applied to the input parameters and so there is not a true equilibrium state. Eurocode factored analysis is considered more applicable to the design of any new structure rather than the stability of the existing.

When considering a target FoS (i.e. acceptable in terms of long term stability) 1.2 is typically used in British Standard analysis.

Geotechnical and Geo-environmental Assessment

As discussed, for the purpose of LE analysis, the retaining wall is considered to be a solid block, therefore, the strength parameters applied to it are somewhat arbitrary but are considered appropriate (i.e. the wall is currently standing).

The parameters for the made ground are based on a combination of factors including the results of the SPTs, laboratory testing and back analysis (again the wall is currently standing).

The parameters for the harbour silt materials is considered typical of such materials. It is noted that in the analysis the silt provides toe weight to the wall and so the drained strength parameters are not critical (i.e. the stability of the silt alone is not considered).

The rock parameters have been derived using RocScience RocLab™ calculations which are based on the strength of the intact rock and the GSI values derived in Section 5.

Table 4 details the drained strength parameters used for the stability analysis.

Table 4: Stability Analysis Parameters

Material Type	Cohesion (kPa)	Friction (°)	Unit Weight (kN/m ³)
Quay Wall	40	45	20
Made Ground	5	34	18
Harbour Silt	0	22	18
MMG	30	39	22
BLF	50	44	22

The groundwater behind the wall in Section 1 is heavily tidally influenced (See Section 5.5). To simplify the analysis the worst case groundwater conditions have been considered.

A surcharge of 10 kN/m² has been applied to the top of the sections as recommended by British Standard. This represents surcharges provided by general plant on the top of the quay wall. It should be noted that this value is considerably lower than the potential point loads provided by the new proposed cranes.

A colour code system of green (acceptable FoS), orange (marginal) and red (i.e. failure) have been used to highlight the stability results.

7.2.2 Stability Analysis Results

Full details of all analysis is included in Appendix H. Based on LE analysis, currently the wall is in a state of marginal stability and that there must be external factors (beyond the capability of LE analysis) acting to increase the overall stability to a level that the wall is not currently failing.

Three scenarios have been analysed for each section. These are as follows;

- Current condition low tide
- Current condition high tide
- Silt dredged from toe of wall

Section 1 (Northern End)

The results for Section 1 are detailed in Table 5 and indicate that the wall is in a state of marginal stability (when considering soil and rock parameters alone). At low tide the wall is marginally stable with the lowest failure plane daylighting through the wall just above the level of the silt in the harbour. The failure mechanism is considered accurate given the wall has been rebuilt in this area.

Table 5: *SLIDE* Analysis Summary (Section 1)

Factor of Safety		
Low Tide	High Tide	Dredged
1.05	1.19	0.79

At high tide the buttressing effect of the water significantly increases the stability (12% increase) as would be expected.

At low tide with the harbour silt removed, the stability significantly reduces (24% reduction) indicating the silt is providing a significant buttressing effect to the toe of the wall.

It is emphasised that the analysis indicates potential instability and suggests likely failure mechanisms rather than showing actual occurrences.

Section 3 (Southern End)

The results for Section 3 are detailed in Table 6. It is evident from this analysis, that there are other factors increasing the stability of the wall (beyond the soil and rock parameters along) as in all instances, the FoS is ≤ 1.0 (i.e. indicating failure). Again in all instances, the failures are close to the wall indicating failure of the wall rather than of the rock.

Table 6: *SLIDE* Analysis Summary (Section 3)

Factor of Safety		
Low Tide	High Tide	Dredged
0.86	1.0	0.86

It is clear that the wall itself is too thin to be providing adequate support to the soils alone and it is likely that the three dimensional buttressing effect along with other external factors are increasing the overall stability.

7.2.3 Discussion

The stability analysis clearly indicates that the stability of the wall in its current state is marginal when considering the soil and to a lesser extent the rock parameters alone (i.e. deep seated rotational failure through the rock is unlikely to occur). It is evident from investigations into the wall that it is relatively thin and has not been adequately designed to modern standards. This is not uncommon of historic quay walls in the south west. Indeed SWG have been involved in the investigation of a number of walls, particularly in the Plymouth and South Hams area where walls have either had inadequate foundations, thicknesses or both.

Using numerical modelling techniques such as Finite Element Analysis or Discrete Element Analysis (beyond SWGs current remit/capability) could be considered to assist with determining the overall stability of the structure although in both instances, it is likely to indicate marginal current stability and certainly inadequate stability in terms of long term future use with large cranes generating large point loads impacting directly on the wall.

On this basis, it is considered that replacing the existing structure with a new, appropriately designed wall / crane supporting structure is necessary.

7.2.4 Remediation Options

Due to the high loads generated by the proposed cranes, any new wall will need to be suitably robust to provide adequate support. Alternatively, a new facing wall could be constructed to support the existing wall and a separate structure built, independent of both walls (or incorporated into the new) to provide a trackway for the new cranes.

Three potential options could be considered for construction of a new wall in front of the existing structure as follows.

- Sheet piled wall. Given the strength of the underlying bedrock, achieving sufficient fixivity with driven sheet piles is likely to be difficult. The crane used to lift boats from the water will impose high loads and it is unlikely that a sheet piled wall alone would provide sufficient support. Anchors would likely be required and given the variable nature of the existing wall, installing anchors may be difficult.
- Construction of solid masonry retaining structure. Given bedrock is relatively close to surface, construction of a new gravity wall could be considered if the water can be kept out and silt removed from the excavation. BH103 encountered poorer ground conditions than the other boreholes potentially due to the faulted contact between the MMG and BLF being present. Some variable settlement could be expected for a gravity wall due to the fault.
- Bored Pile Wall/ Crane Deck. Potentially the most straight forward option whereby a new facing wall is constructed in-front of the existing wall coupled with piles through the trackway/ crane working area to provide a piled trackway on which cranes operate. The faulted contact between the MMG and BLF striking east-west through the centre of the wall (BH103) would mean bored piles are likely to have variable lengths.

Following the design of any new structures and or remedial measures to the existing structures, it is recommended the global stability is re-analysed based on the new geometry.

7.3 Foundation and Pile Design

The MMG and BLF bedrock will provide adequate support for any new structure. Foundations for new structures.

7.3.1 Foundations

If a gravity wall is to be used, an allowable bearing capacity of 330 kN/m² has been calculated (using for the MMG (weakest materials) for a 5.0m wide foundation, using Equation 5.7 Wyllie (2009). CIRIA C570 (2001), indicates that settlements rarely exceed 20mm for relatively light loads such as this on MMG materials.

7.3.2 Piles

If bored piles were to be utilised for the basement perimeter, it would make sense to utilise them for the internal columns to support the centre of the structure as they will provide a higher capacity than traditional pad foundations. Piles should be installed into the upper levels of the MMG.

Preliminary pile capacity from skin friction Q_s has been calculated for a 0.6m diameter pile using the equation:

$Q_s = \alpha \times \beta \times q_{uc} \times A_s / F$ (Tomlinson, 2001, p302) with parameters defined as follows;

- α a factor applied to the soil / rock shear strength (taken as 0.2 for the MMG),
- q_{uc} is the unconfined compressive rock strength with a value of 6000 kPa used for the purposes of this assessment. This is the average value of all PLT and UCS tests.
- β is the rock socket correction factor (taken as 0.8 for the MMG, based on an average RQD of 63%),
- A_s is the shaft area
- F is a factor of safety, taken as 3 for the purposes of this assessment.

Based on the preliminary design of a 0.6m diameter pile and 4.0m rock socket, the preliminary capacity of the pile has been determined to be 2590 kN based on a FoS of 3. This is considered a preliminary working load for piles with a relatively short rock socket.

Where piles are free standing (i.e. anchors are not utilised), the embedment of the pile is typically twice the retained height, subsequently longer rock sockets would allow higher capacity. An anchored capping beam forming the top of a new quay wall could be used to reduce the length of the piles.

Final pile design should take into account additional factors such as the soil /rock effective stress parameters, pile settlement and structural limits on settlement acceptability, negative skin friction from down-drag of the overlying fill, lateral pressures, the effects interaction between neighbouring piles and pile group effects.

7.4 Retaining Wall Design

The parameters used in the stability analysis detailed in Table 4 can generally be used for the design of any new retaining structure.

Due to the high variability of the made ground, it is recommended that a cohesion value of 0 kPa and friction angle 30° is used for the design of any new structure.

Any eccentric loads generated by overturning moments will need to be kept below the allowable bearing capacity detailed in Section 7.3.1.

7.5 Re-use of Materials

Seven PSD sieves were undertaken on the made ground materials (see Figure 2). The sieves indicate the materials would generally be classified as either Class 1B uniformly graded granular materials or Class 2C stony cohesive in accordance with Highways Agency, Specification for Highways Works (2016). One sample (BH103 2.8m), would be Classed as 2A wet cohesive materials.

Given the granular nature of the majority of the near surface materials, the natural moisture content is expected to be close to optimum although it is noted that the deeper materials

have significantly higher moisture content than the near surface material due to tides. The lower moisture content values (12-14% approx.) are expected to be optimum.

7.6 Modulus of Sub-Grade Reaction

Modulus of sub-grade reaction has been calculated for each stage of the two plate load tests undertaken beneath the existing concrete slab.

As would be expected for non-engineered fill materials the values are highly variable ranging from 9059 to 79010 kPa/m.

7.7 Sulphate Classification

The 9 no soluble sulphate test results indicate concentrations of between 0.05 and 1.42g/l, with pH values of between 7.8 and 10 (average 8.5). Taking the average of the two sulphate concentrations as recommended by (BRE SD1, 2005), concrete should be designed to a Design Sulphate Class of DS-2, and ACEC Class AC-2.

Given the marine environment, marine concrete will be required.

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8 REFERENCES AND BIBLIOGRAPHY

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9 LIMITATIONS

This report has been prepared by SWG solely for the benefit of West Somerset and Taunton Deane Borough Council. It shall not be relied upon or transferred to any third party without the prior written authorisation of SWG.

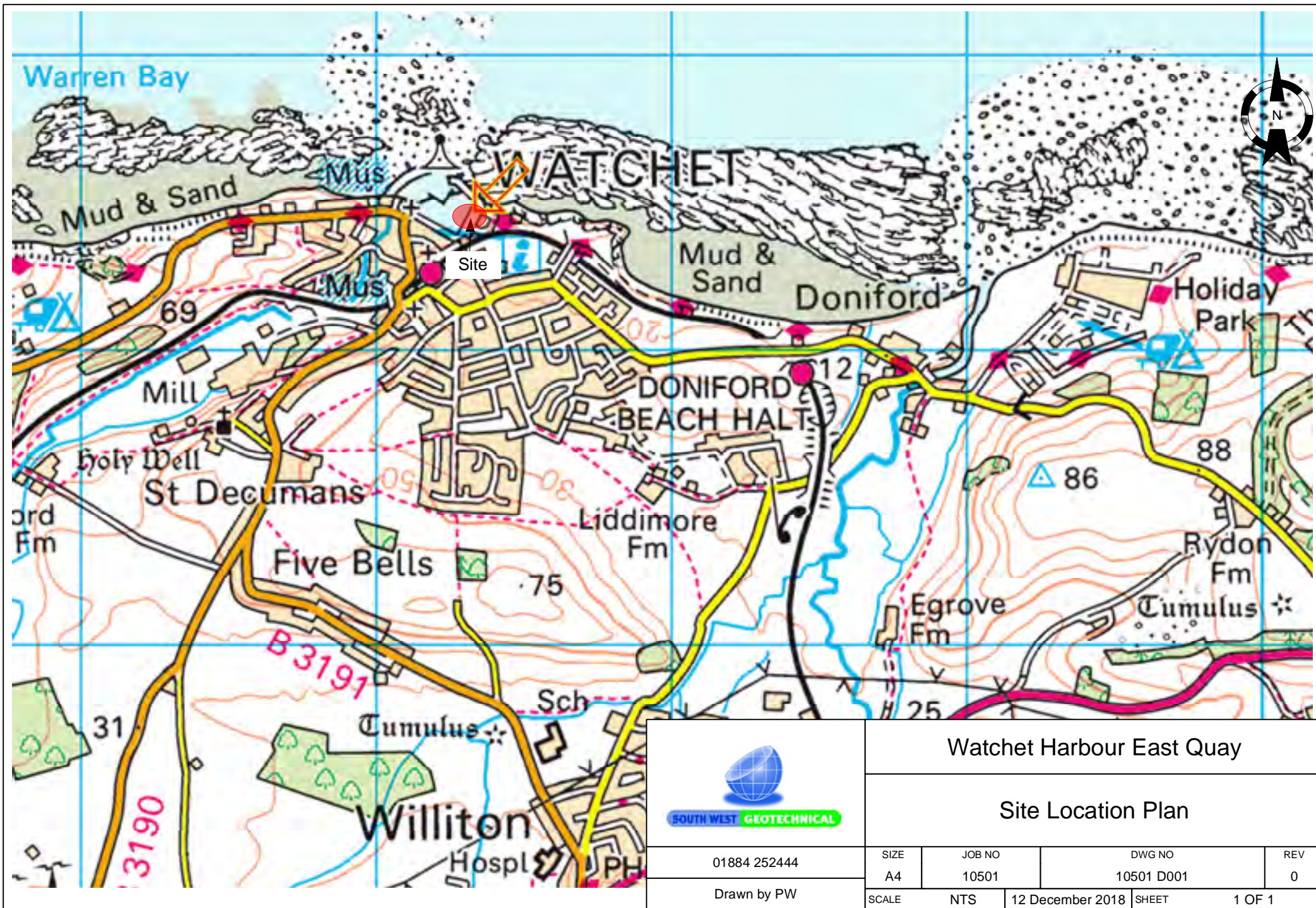
All information given in this report is based on the ground conditions encountered during the site work, and on the results of laboratory and field tests performed during the investigation. However, there may be conditions at the site which have not been taken into account, such as unpredictable soil strata, contaminant concentrations, and water conditions between or below exploratory holes.

It should be noted that groundwater levels usually vary due to seasonal and/or other effects and may at times differ to those measured during the investigation.

British Standards Institute (BSI, 2015) ordinarily recommends that laboratory measurements of strength in cohesive soils be undertaken only on high-quality (Category 'A') undisturbed samples, necessitating the use of wire-line drilling or thin-wall samples tubes. However, given the relatively low geotechnical risk presented and the low probability of being able to recover Category 'A' samples from the anticipated strata, it is considered that the use of such techniques is neither appropriate nor cost-effective.

Appendix A

Site Location Plan





Appendix B






Geology Report

Geology 1:50,000 Maps Legends








Artificial Ground and Landslip






Map Colour	Lex Code	Rock Name	Rock Type	Min and Max Age
	MGR	Made Ground (Undivided)	Artificial Deposit	Not Supplied - Holocene
	SLIP	Landslide Deposit	Clay	Not Supplied - Quaternary

Superficial Geology

Map Colour	Lex Code	Rock Name	Rock Type	Min and Max Age
	ALV	Alluvium	Clay, Silt, Sand and Gravel	Not Supplied - Holocene
	HEAD	Head	Clay, Silt, Sand and Gravel	Not Supplied - Quaternary
	BTFU	Beach and Tidal Flat Deposits (Undifferentiated)	Clay, Silt, Sand and Gravel	Not Supplied - Quaternary
	MDU	Marine Deposits	Gravel	Not Supplied - Quaternary
	RTDU	River Terrace Deposits (Undifferentiated)	Sand and Gravel	Not Supplied - Quaternary

Bedrock and Faults

Map Colour	Lex Code	Rock Name	Rock Type	Min and Max Age
	LPBL	Langport Member and Blue Lias Formation (Undifferentiated)	Mudstone and Limestone, Interbedded	Not Supplied - Rhaetian
	WBCT	Westbury Formation and Cotham Member (Undifferentiated)	Mudstone and Limestone, Interbedded	Not Supplied - Rhaetian
	PNG	Penarth Group	Mudstone and Limestone, Interbedded	Not Supplied - Rhaetian
	BLI	Blue Lias Formation	Mudstone and Limestone, Interbedded	Not Supplied - Rhaetian
	LPBLC	Langport Member, Blue Lias Formation and Charmouth Mudstone Formation (Undifferentiated)	Mudstone and Limestone, Interbedded	Not Supplied - Rhaetian
	LPBLC	Langport Member, Blue Lias Formation and Charmouth Mudstone Formation (Undifferentiated)	Mudstone	Not Supplied - Rhaetian
	BLCD	Blue Lias Formation, Charmouth Mudstone	Mudstone	Not Supplied - Rhaetian

Map Colour	Lex Code	Rock Name	Rock Type	Min and Max Age
	BAN	Blue Anchor Formation	Mudstone	Not Supplied - Norian
	MMG	Mercia Mudstone Group	Mudstone	Not Supplied - Early Triassic
	MMG	Mercia Mudstone Group	Mudstone and Halite-stone	Not Supplied - Early Triassic
	MMG	Mercia Mudstone Group	Sandstone	Not Supplied - Early Triassic
		Faults		

Geology 1:50,000 Maps

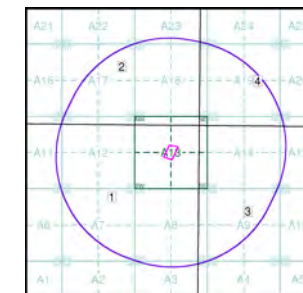
This report contains geological map extracts taken from the BGS Digital Geological map of Great Britain at 1:50,000 scale and is designed for users carrying out preliminary site assessments who require geological maps for the area around the site. This mapping may be more up to date than previously published paper maps.

The various geological layers - artificial and landslip deposits, superficial geology and solid (bedrock) geology are displayed in separate maps, but superimposed on the final 'Combined Surface Geology' map. All map legends feature on this page. Not all layers have complete nationwide coverage, so availability of data for relevant map sheets is indicated below.

Geology 1:50,000 Maps Coverage

Map ID: 3	Map ID: 4
Map Sheet No: 295	Map Sheet No: 279
Map Name: Taunton	Map Name: Weston-super-M
Map Date: 1984	Map Date: 1980
Bedrock Geology: Available	Bedrock Geology: Available
Superficial Geology: Available	Superficial Geology: Available
Artificial Geology: Available	Artificial Geology: Available
Faults: Not Supplied	Faults: Not Supplied
Landslip: Available	Landslip: Available
Rock Segments: Not Supplied	Rock Segments: Not Supplied
Map ID: 1	Map ID: 2
Map Sheet No: 294	Map Sheet No: 278
Map Name: Dulverton	Map Name: Minehead
Map Date: 1969	Map Date: 1997
Bedrock Geology: Available	Bedrock Geology: Available
Superficial Geology: Available	Superficial Geology: Available
Artificial Geology: Available	Artificial Geology: Available
Faults: Not Supplied	Faults: Not Supplied
Landslip: Available	Landslip: Available
Rock Segments: Not Supplied	Rock Segments: Not Supplied

Geology 1:50,000 Maps - Slice A



Order Details:

Order Number: 189169426_1_1
Customer Reference: 10501
National Grid Reference: 307360, 143400
Slice: A
Site Area (Ha): 1.02
Search Buffer (m): 1000

Site Details:

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Artificial Ground and Landslip

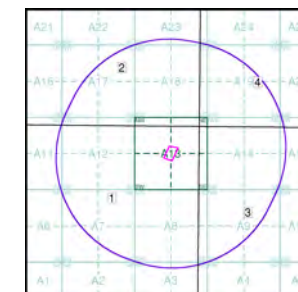
Artificial ground is a term used by BGS for those areas where the ground surface has been significantly modified by human activity. Information about previously developed ground is especially important, as it is often associated with potentially contaminated material, unpredictable engineering conditions and unstable ground.

Artificial ground includes:

- Made ground - man-made deposits such as embankments and spoil heaps on the natural ground surface.
- Worked ground - areas where the ground has been cut away such as quarries and road cuttings.
- Infilled ground - areas where the ground has been cut away then wholly or partially backfilled.
- Landscaped ground - areas where the surface has been reshaped.
- Disturbed ground - areas of ill-defined shallow or near surface mineral workings where it is impracticable to map made and worked ground separately.

Mass movement (landslip) deposits on BGS geological maps are primarily superficial deposits that have moved down slope under gravity to form landslips. These affect bedrock, other superficial deposits and artificial ground. The dataset also includes foundered strata, where the ground has collapsed due to subsidence.

Artificial Ground and Landslip Map - Slice A



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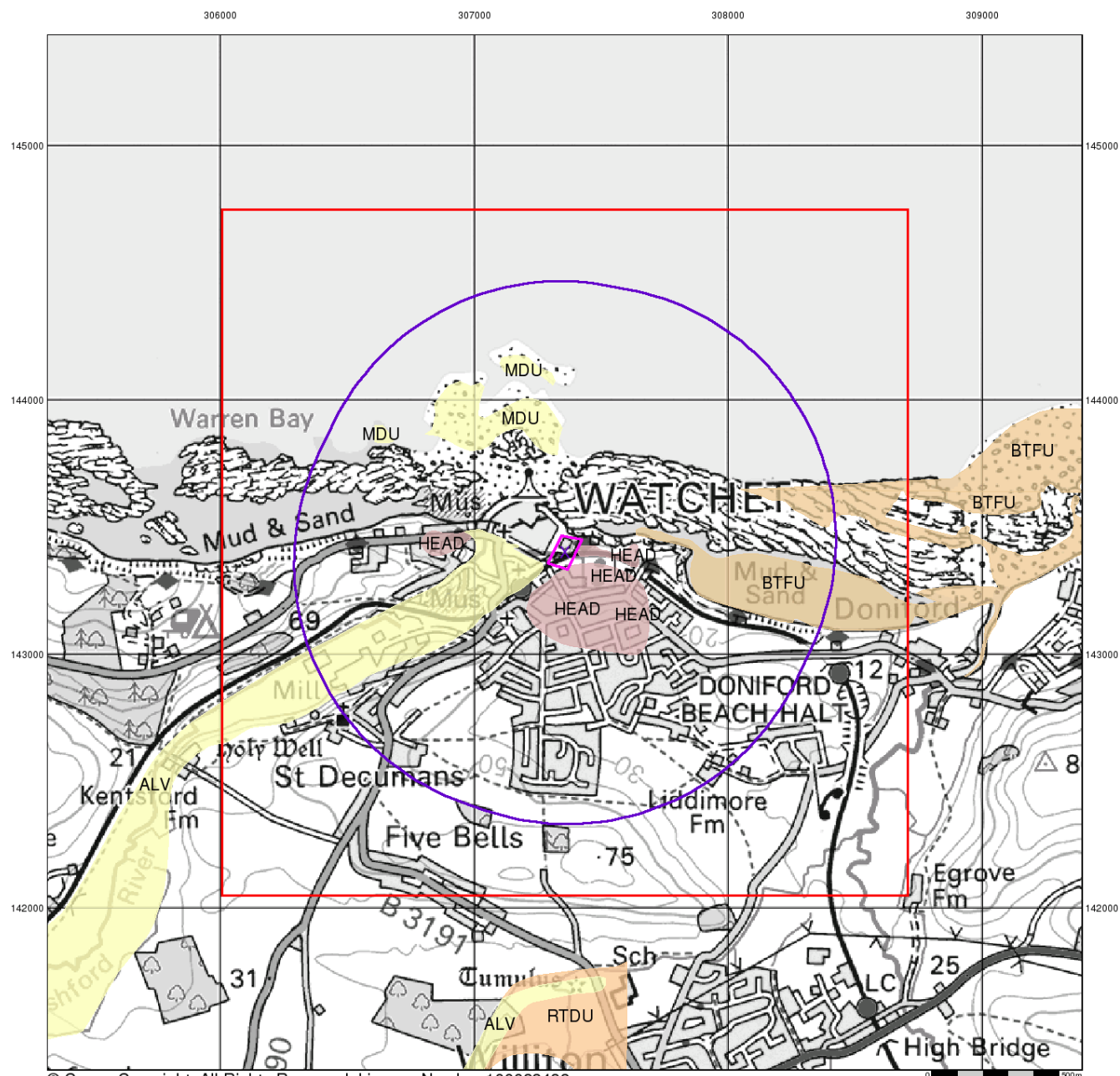
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 Search Buffer (m): 1000

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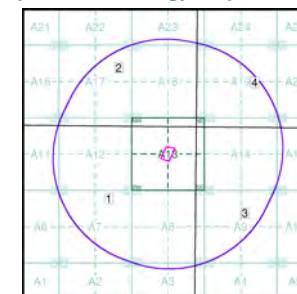
Superficial Geology

Superficial Deposits are the youngest geological deposits formed during the most recent period of geological time, the Quaternary, which extends back about 1.8 million years from the present.

They rest on older deposits or rocks referred to as Bedrock. This dataset contains Superficial deposits that are of natural origin and 'in place'. Other superficial strata may be held in the Mass Movement dataset where they have been moved, or in the Artificial Ground dataset where they are of man-made origin.

Most of these Superficial deposits are unconsolidated sediments such as gravel, sand, silt and clay, and onshore they form relatively thin, often discontinuous patches or larger spreads.

Superficial Geology Map - Slice A



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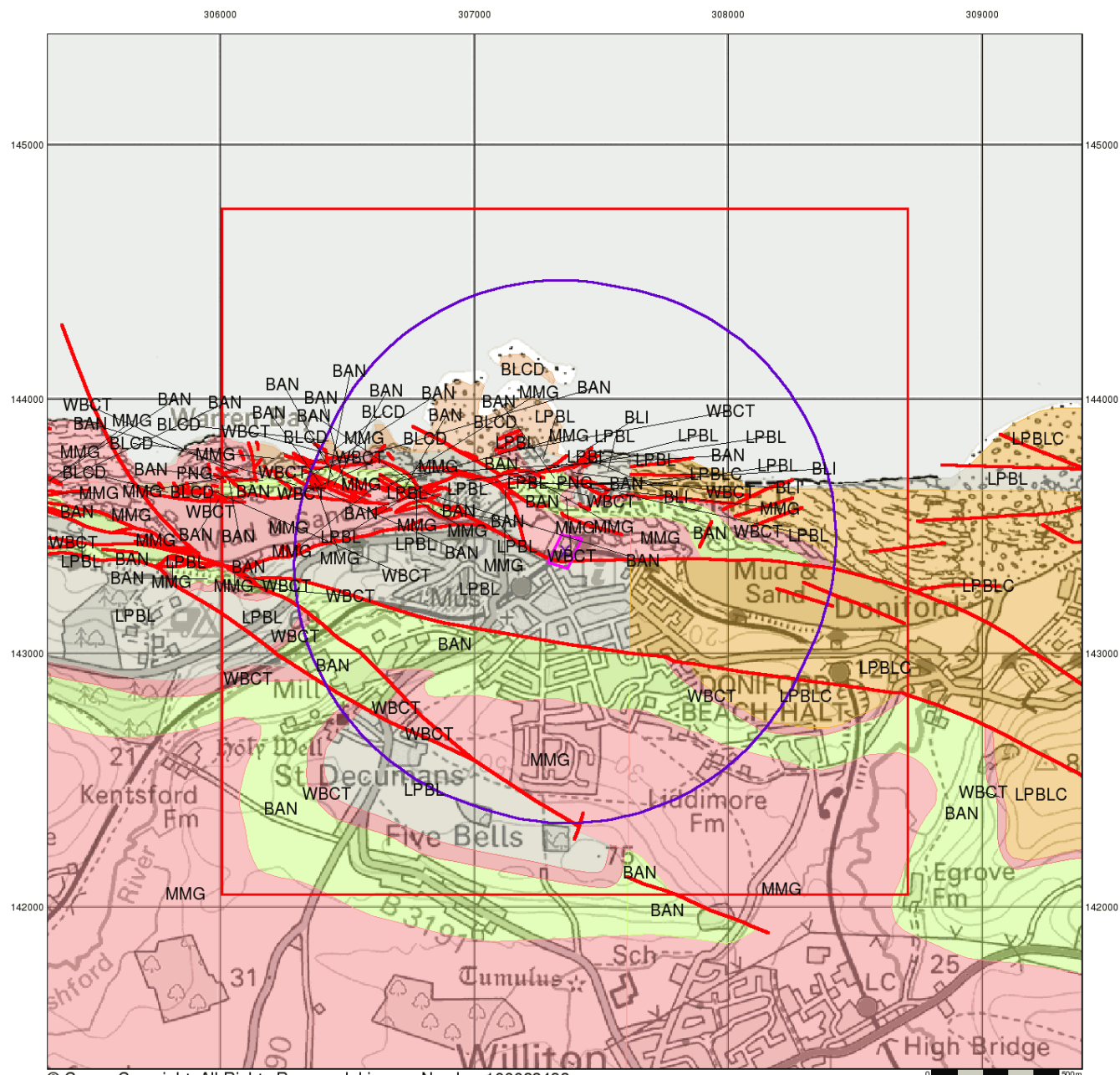
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Bedrock and Faults

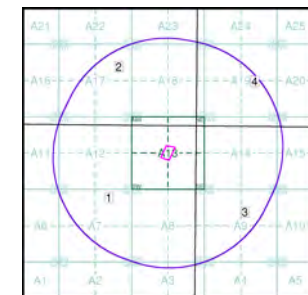
Bedrock geology is a term used for the main mass of rocks forming the Earth and are present everywhere, whether exposed at the surface in outcrops or concealed beneath superficial deposits or water.

The bedrock has formed over vast lengths of geological time ranging from ancient and highly altered rocks of the Proterozoic, some 2500 million years ago, or older, up to the relatively young Pliocene, 1.8 million years ago.

The bedrock geology includes many lithologies, often classified into three types based on origin: igneous, metamorphic and sedimentary.

The BGS Faults and Rock Segments dataset includes geological faults (e.g. normal, thrust), and thin beds mapped as lines (e.g. coal seam, gypsum bed). Some of these are linked to other particular 1:50,000 Geology datasets, for example, coal seams are part of the bedrock sequence, most faults and mineral veins primarily affect the bedrock but cut across the strata and post date its deposition.

Bedrock and Faults Map - Slice A



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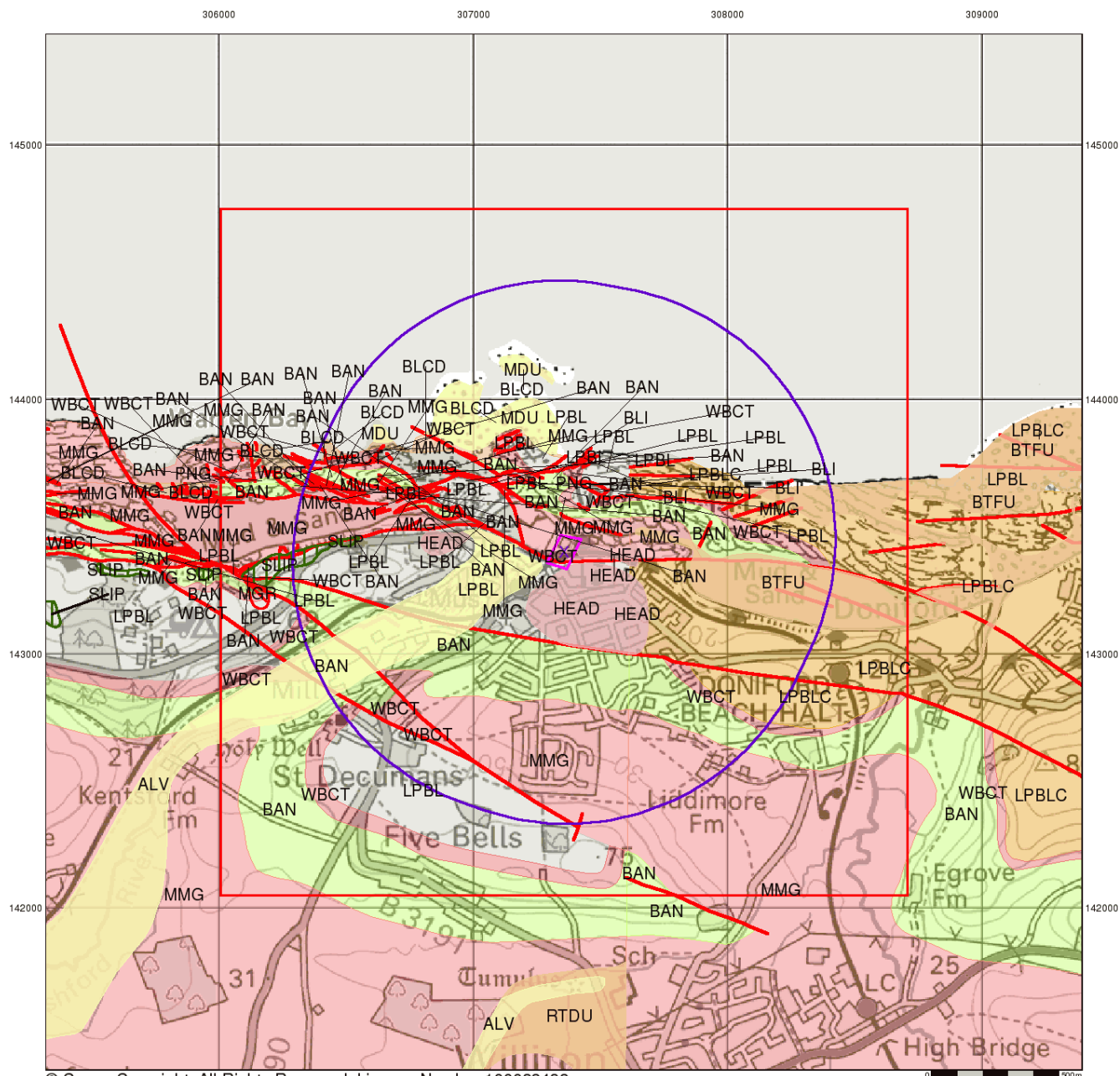
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Combined Surface Geology

The Combined Surface Geology map combines all the previous maps into one combined geological overview of your site.

Please consult the legends to the previous maps to interpret the Combined "Surface Geology" map.

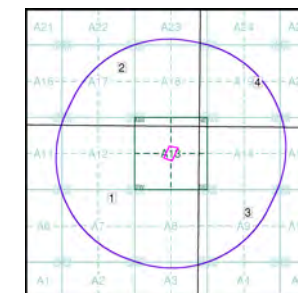
Additional Information

More information on 1:50,000 Geological mapping and explanations of rock classifications can be found on the BGS website. Using the LEX Codes in this report, further descriptions of rock types can be obtained by interrogating the 'BGS Lexicon of Named Rock Units'. This database can be accessed by following the 'Information and Data' link on the BGS website.

Contact

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Kingsley Dunham Centre
Keyworth
Nottingham
NG12 5GG
Telephone: 0115 936 3143
Fax: 0115 936 3276
email: xxxxxxxx@xxx.xx.xx
website: www.bgs.ac.uk

Combined Geology Map - Slice A



Order Details:

Order Number: 189169426_1_1
Customer Reference: 10501
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Appendix C

Exploratory Hole Location Plan



EXPLORATORY HOLE LOCATION PLAN

WATCHET HARBOUR

SCALE	PROJECT NO
NTS	10501



Appendix D

Exploratory Hole Logs and Photos

KEY TO EXPLORATORY HOLE LOGS

SAMPLING

Undisturbed

U	Driven tube sample (Blow count recorded in results column i.e. U = 20)
TW	Pushed thin wall tube sample
P	Pushed piston sample
L	Liner sample
CBR	CBR mould sample
BLK	Block sample
WS	Window sample
CS	Core sample

Disturbed

D	Small sample
B	Bulk sample

Other

W	Water sample
G	Gas sample
ES	Soil sample for environmental analysis
EW	Water sample for environmental analysis

IN-SITU TESTING

SPT S or SPT C	Standard Penetration Test, open shoe (S) or solid cone (C)
----------------	--

As defined in BS 1377 : Part 9 (1990). Standard Penetration Test (SPT): a 50mm split spoon or solid cone sampler is driven 450mm into the base of the borehole using a 63.5 kg hammer with a 760mm drop. The penetration resistance (e.g. 21) is expressed as the N-value, and represents the number of blows required to obtain 300mm penetration below an initial seating drive of 150mm.

The depth on the borehole/ trial pit record is that of the start and end of the test. Where full penetration for the test has not been achieved, the final penetration depth is recorded.

HVP (kPa)	In-situ Hand Vane shear strength: a hand shear vane test (or average of a series), conducted on undisturbed samples or within trial pits.
-----------	---

GIVN (kPa)	Geonor in-situ vane shear strength carried out in base of borehole or self bored hole
------------	---

VN (kPa)	Hand Vane shear strength, conducted on disturbed or remoulded samples.
PP (kg/cm ²)	Pocket penetrometer test: a pocket Penetrometer reading (or average of a series). If reported in kPa, the value has been converted to an equivalent undrained shear strength.

Ik	In situ permeability test
ICBR	In-situ CBR test
IPBT	In-situ plate bearing test
IPST	In-situ plate settlement test

All test results are provided in Results column

DRILLING RECORDS

TCR	Total Core Recovery %
SCR	Solid Core Recovery %
RQD	Rock Quality Designation %
FI	Fracture Spacing mm. Minimum, typical and maximum spacings are recorded.

GR002

Version 6

27/07/2018

GR002 Key to exploratory records

GROUNDWATER



Groundwater Strike



Groundwater level after standing time

INSTALLATION

Standpipe/ piezometer

Details of standpipe/piezometer installations are given on the left side of the log. The column shows installed instrument depths including slotted pipe section or tip depth, response zone filter material type and layers of backfill.

SP	Standpipe
SPIE	Standpipe piezometer
PPIE	Pneumatic piezometer
EPIE	Electronic piezometer

NOTES

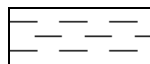
Water level observations of discernible entries during the advancing of the exploratory hole are given at the foot of the log and in the Legend column. The term "none observed" is used where no discrete entries are identified although this does not necessarily indicate that the hole has not been advanced below groundwater level. Under certain conditions groundwater cannot be observed, for instance, drilling with water flush or over water, or boring at a rate much faster than water can make its way into the borehole.

The declination of bedding and joints is given with respect to the normal to the core axis. Thus in a vertical borehole this will be the dip.

Remarks on chiselling times can be affected by a variety of factors not always related to the geotechnical properties of the strata. Chiselling records are given at the foot of the log.

The assessment of SCR, RQD and Fracture Spacing excludes artificial fractures.

KEY TO SOIL LEGENDS



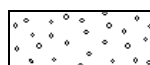
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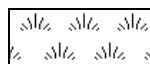
SILT



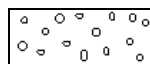
SAND



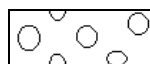
GRAVEL



PEAT



COBBLES



BOULDERS



TOPSOIL



MADE GROUND

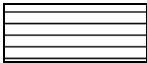

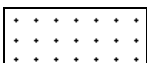
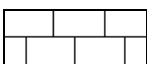
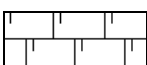

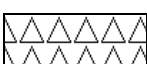
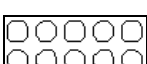
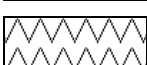
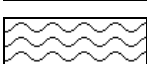
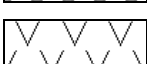
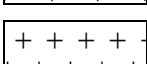
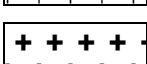
GR002

Version 6




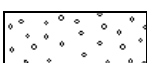
27/07/2018

GR002 Key to exploratory records

KEY TO ROCK LEGENDS


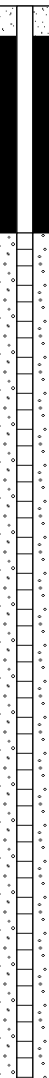


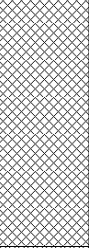
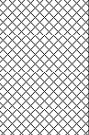

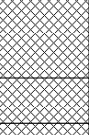
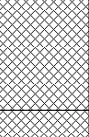
	MUDSTONE
	SILTSTONE
	SANDSTONE
	LIMESTONE
	CHALK
	COAL
	BRECCIA
	CONGLOMERATE
	FINE GRAINED METAMORPHIC
	MEDIUM/COARSE GRAINED METAMORPHIC
	FINE GRAINED IGNEOUS
	MEDIUM GRAINED IGNEOUS
	COARSE GRAINED IGNEOUS

KEY TO BACKFILL LEGENDS


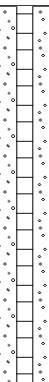


	BENTONITE
	ARISINGS
	SAND
	GRAVEL

REFERENCES

BS 1377 : 1990 : British Standard Methods of test for soils for civil engineering purposes. British Standards Institution.
 BS 5930 : 1999 : Code of practice for site investigations. British Standards Institution.

				<h1>Borehole Log</h1>				Borehole No. BH101 Sheet 1 of 2	
Project Name: Watchet Harbour				Project No. 10501		Co-ords:		Hole Type CP+RC	
Location: Somerset				Level: 8.30		Scale 1:50		Logged By PW	
Client: Taunton Dean Bourough Council				Dates: 06/11/2018					
Well	Water Strikes	Sample and In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description	
		Depth (m)	Type	Results					
					0.10	8.20		Tarmac	1
	0.40 0.40	D ES			0.50	7.80			
	1.20 - 1.65 1.20 1.50	D SPT D	N=9 (2,2/3,2,2,2)					(MADE GROUND). Firm reddish brown sandy gravelly clay. Tending to very clayey very sandy gravel. Gravel is fine to coarse subangular mudstone and limestone fragments. Rare brick fragments.	2
	2.70 - 3.15 2.70 - 3.60 2.70	D B SPT	N=16 (2,2/1,5,5,5)	2.70	5.60			(MADE GROUND). Medium dense orange brown silty sandy gravel. Gravel is fine to coarse subangular mudstone fragments.	
	3.70 - 3.95 3.70	D SPT	50 (2,2/50 for 85mm)	3.60	4.70			(MADE GROUND). Soft grey sandy slightly gravelly clay. Gravel is fine to coarse subrounded mudstone and sandstone fragments.	
	4.50 4.50	D SPT	N=24 (2,3/6,5,7,6)	3.95 4.15	4.35 4.15		(MADE GROUND). Strong grey limestone boulder.	4	
				4.70	3.60		(MADE GROUND). Soft to firm grey brown sandy gravelly clay. Tending to very clayey very sandy gravel. Gravel is fine to coarse subangular and subrounded mudstone fragments.		
	5.50	D		5.00	3.30		(MADE GROUND). Stiff pale green slightly gravelly clay/silt.		
								(MADE GROUND). Loose light brown very clayey very sandy gravel with rare mudstone cobbles.	5
	6.00 - 7.00 6.00	B SPT	N=23 (2,3/7,5,5,6)	5.80 6.00	2.50 2.30	(MADE GROUND?). Medium dense? Grey green very clayey sandy gravel. Gravel is fine to medium subangular mudstone and rare subrounded mudstone fragments.			
7.00	SPT	50 (25 for 5mm/50 for 10mm)	7.00	1.30	Medium dense grey green and red brown clayey sandy GRAVEL. Gravel is fine to coarse angular mudstone fragments. (RESIDUAL SOIL).				
							Very weak to weak, grey green and red brown, slightly weathered, MUDSTONE with occasional fine (1-2mm) gypsum veins. (MERCIA MUDSTONE GROUP).	6	
							Fractures are closely to medium spaced (80, 200, 380), undulating smooth and rough, dipping at 20-30° (J1) and 45° (J2), no infill.	7	
									8
									9
									10
Remarks Location CAT scanned and inspection pit hand excavated to 1.2m prior to drilling. Hole drilled by dynamic sampling to 7.20mbgl, then continued by rotary coring. Monitoring well installed to base of hole.									



				<h1 style="text-align: center;">Rotary Core Log</h1>				Borehole No. BH101			
Project Name: Watchet Harbour				Project No. 10501		Co-ords:		Sheet 2 of 2 Hole Type CP+RC			
Location: Somerset				Level: 8.30		Scale 1:50					
Client: Taunton Dean Bourough Council				Dates: 06/11/2018 - 07/11/2018		Logged By PW					
Well	Water Strikes	Depth (m)	Type /FI	Coring			Depth (m)	Level (m AOD)	Legend	Stratum Description	
				TCR	SCR	RQD					
		10.00 - 11.50	4	100	95	75	12.50	-4.20		Weak to medium strong becoming weak below 12.30m, reddy brown, fresh locally slightly weathered, MUDSTONE with occasional fine gypsum veins (MERCIA MUDSTONE GROUP). Fractures are closely to widely spaced (80, 300, 750), undulating rough and smooth, dipping at 25° (J1) and 45° (J2), no infill.	11
		11.50 - 12.50		80	64	43					12
			13								
										End of Borehole at 12.500m	14
											15
											16
											17
											18
											19
											20
Remarks Location CAT scanned and inspection pit hand excavated to 1.2m prior to drilling. Hole drilled by dynamic sampling to 7.20mbgl, then continued by rotary coring. Monitoring well installed to base of hole.											


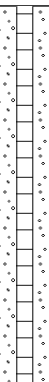




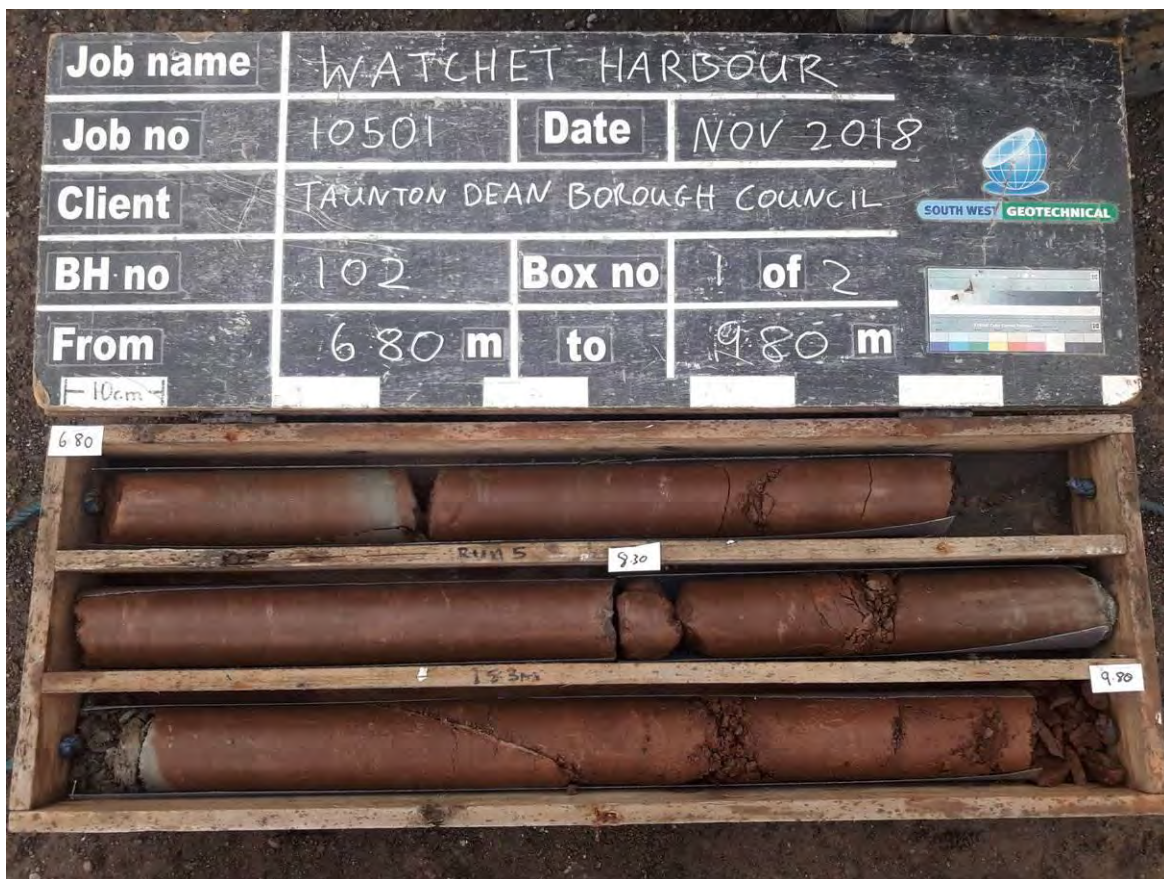
BH101: 7.20 – 10.0m



BH101: 10.0 – 12.50m



				<h1 style="text-align: center;">Rotary Core Log</h1>				Borehole No. BH102							
Project Name: Watchet Harbour				Project No. 10501		Co-ords:		Sheet 2 of 2 Hole Type CP+RC							
Location: Somerset				Level: 8.20		Scale 1:50									
Client: Taunton Dean Bourough Council				Dates: 07/11/2018 - 08/11/2018		Logged By PW									
Well	Water Strikes	Depth (m)	Type /FI	Coring			Depth (m)	Level (m AOD)	Legend	Stratum Description					
				TCR	SCR	RQD									
		9.80 - 11.30	50	93	48	20	12.50	-4.30		Weak locally very weak (9.3-9.8m), red brown and locally grey green slightly weathered MUDSTONE. (MERCIA MUDSTONE GROUP). Fractures are closely to medium spaced (80, 300, 520), undulating smooth, dipping at 15-20° (J1) and 50° (J2), rare 2-3mm gypsum infill.	11				
			5												12
			50												
		11.30 - 12.50	5	100	100	91									
End of Borehole at 12.500m											13				
											14				
											15				
											16				
											17				
											18				
											19				
											20				
Remarks Location CAT scanned and inspection pit hand excavated to 1.2m prior to drilling. Hole drilled by dynamic sampling to 6.80mbgl, then continued by rotary coring. Monitoring well installed to base of hole.															
															



BH102: 6.80 – 9.80m



BH102: 9.80 – 12.50m

Project Name: Watchet Harbour

Project No.
10501

Co-ords:

Hole Type
CP+RC

Location: Somerset

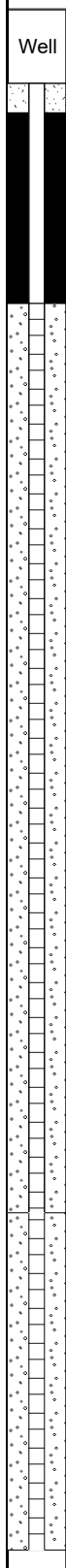

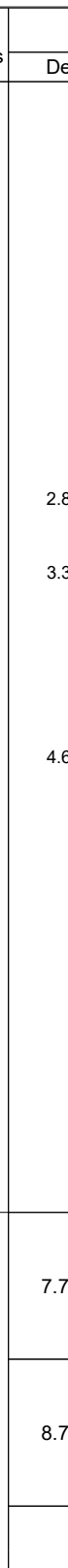
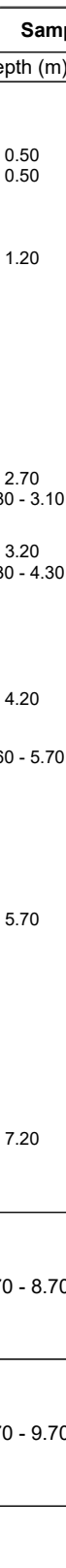

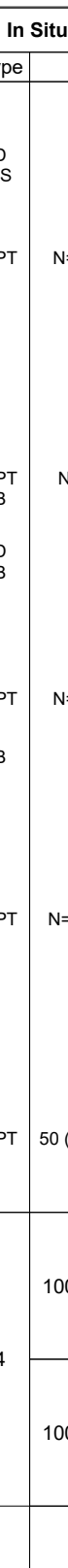


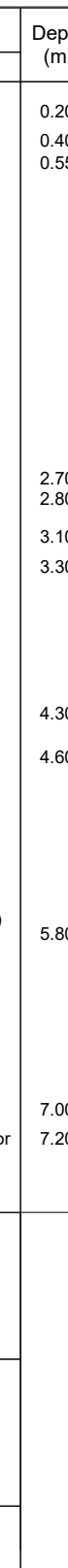
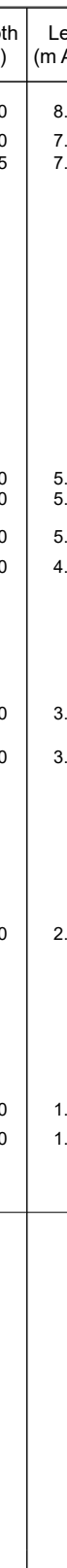
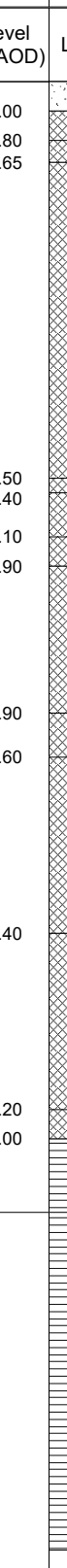

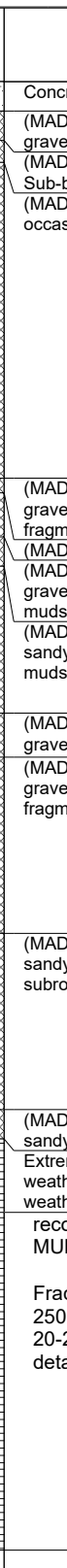
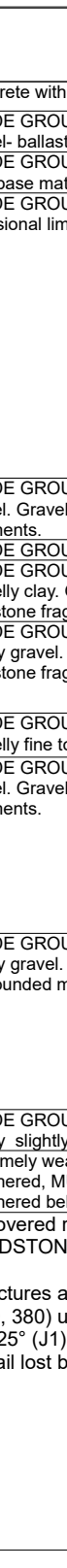
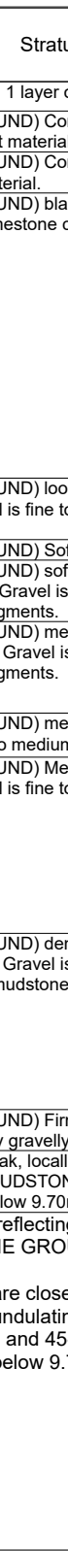
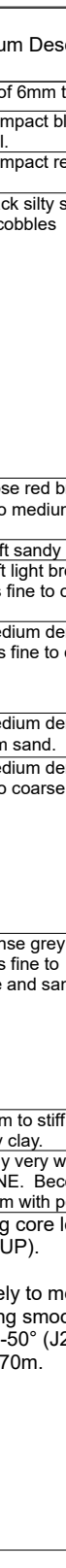
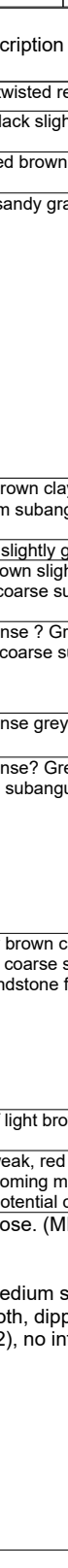
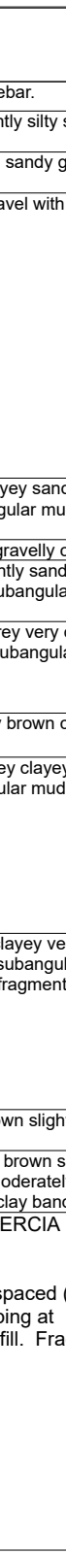
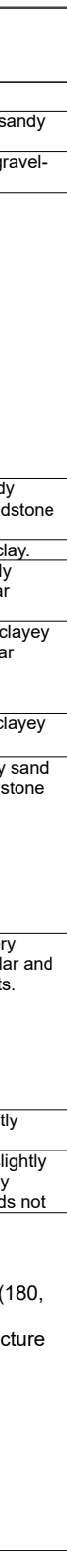

Level: 8.20

Scale
1:50

Client: Taunton Dean Bourough Council

Dates: 09/11/2018


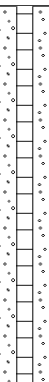


Logged By
PW

Well	Water Strikes	Sample and In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description			
		Depth (m)	Type	Results							
		0.50 0.50	D ES	N=10 (6,3/2,2,3,3)	0.20 0.40 0.55	8.00 7.80 7.65		Concrete with 1 layer of 6mm twisted rebar. (MADE GROUND) Compact black slightly silty sandy gravel- ballast material. (MADE GROUND) Compact red brown sandy gravel- Sub-base material. (MADE GROUND) black silty sandy gravel with occasional limestone cobbles	1		
		1.20			SPT	4.30		3.90		(MADE GROUND) loose red brown clayey sandy gravel. Gravel is fine to medium subangular mudstone fragments. (MADE GROUND) Soft sandy slightly gravelly clay. (MADE GROUND) soft light brown slightly sandy gravelly clay. Gravel is fine to coarse subangular mudstone fragments. (MADE GROUND) medium dense ? Grey very clayey sandy gravel. Gravel is fine to coarse subangular mudstone fragments.	2
		2.70 2.80 - 3.10			SPT B	2.70 2.80		5.50 5.40			
		3.20 3.30 - 4.30	D B	3.10 3.30	5.10 4.90		(MADE GROUND) dense grey brown clayey very sandy gravel. Gravel is fine to coarse subangular and subrounded mudstone and sandstone fragments.	4			
		4.20 4.60 - 5.70	SPT B	4.30 4.60	3.90 3.60				(MADE GROUND) Firm to stiff light brown slightly sandy slightly gravelly clay. Extremely weak, locally very weak, red brown slightly weathered, MUDSTONE. Becoming moderately weathered below 9.70m with potential clay bands not recovered reflecting core lose. (MERCIA MUDSTONE GROUP).	5	
		5.70	SPT	5.80	2.40						Fractures are closely to medium spaced (180, 250, 380) undulating smooth, dipping at 20-25° (J1) and 45-50° (J2), no infill. Fracture detail lost below 9.70m.
		7.20	SPT	7.00 7.20	1.20 1.00						
											
											
											
											
											
											
											
											
											
											
											

Remarks



Location CAT scanned and inspection pit hand excavated to 1.2m prior to drilling. Hole drilled by dynamic sampling to 7.70mbgl, then continued by rotary coring. Monitoring well installed to base of hole.




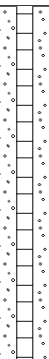

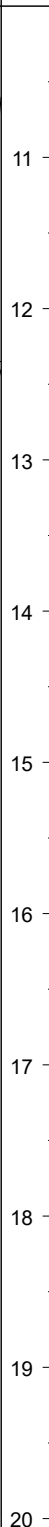
				<h1 style="text-align: center;">Rotary Core Log</h1>				Borehole No. BH103			
Project Name: Watchet Harbour				Project No. 10501		Co-ords:		Sheet 2 of 2 Hole Type CP+RC			
Location: Somerset				Level: 8.20		Scale 1:50					
Client: Taunton Dean Bourough Council				Dates: 09/11/2018 - 12/11/2018		Logged By PW					
Well	Water Strikes	Depth (m)	Type /FI	Coring			Depth (m)	Level (m AOD)	Legend	Stratum Description	
				TCR	SCR	RQD					
		9.70 - 11.20	D SPT	30	8	0	12.50	-4.30		Extremely weak, locally very weak, red brown slightly weathered, MUDSTONE. Becoming moderately weathered below 9.70m with potential clay bands not recovered reflecting core lose. (MERCIA MUDSTONE GROUP). Fractures are closely to medium spaced (180, 250, 380) undulating smooth, dipping at 20-25° (J1) and 45-50° (J2), no infill. Fracture detail lost below 9.70m.	11
		11.20 - 12.50		38	8	0					12
		12.50 - 12.95 N=44 (25 for 80mm/13,15,8,8)									
										End of Borehole at 12.500m	14
											15
											16
											17
											18
											19
											20
Remarks Location CAT scanned and inspection pit hand excavated to 1.2m prior to drilling. Hole drilled by dynamic sampling to 7.70mbgl, then continued by rotary coring. Monitoring well installed to base of hole.											



BH103: 7.70 – 12.50m

						<h1>Borehole Log</h1>				Borehole No. BH104 Sheet 1 of 2	
Project Name: Watchet Harbour						Project No. 10501		Co-ords:		Hole Type CP+RC	
Location: Somerset						Level: 8.35		Scale 1:50		Logged By PW	
Client: Taunton Dean Bourough Council						Dates: 13/11/2018					
Well	Water Strikes	Sample and In Situ Testing			Depth (m)	Level (m AOD)	Legend	Stratum Description			
		Depth (m)	Type	Results							
					0.20	8.15		Concrete with 1 layer of 6mm twisted rebar.			
		0.50	D		0.60	7.75		(MADE GROUND) Compact black slightly silty sandy gravel- ballast material.			
		0.50	ES		0.80	7.55		(MADE GROUND) dense grey slightly sandy gravel and cobbles of limestone and quartzite.			
		1.20	SPT	N=17 (1,2/5,8,2,2)				(MADE GROUND) loose black sandy gravel of ash and clinker with brick and mortar fragments at 1.40m.	1		
		1.80	D		1.70	6.65		(MADE GROUND) firm grey slightly sandy gravelly clay with occasional brick and limestone cobbles. Tending to very clayey very sandy gravel.	2		
		2.70	SPT	N=7 (2,3/1,2,2,2)					3		
		3.20 - 4.20	B		3.30	5.05		(MADE GROUND) soft light brown slightly sandy gravelly clay. Gravel is fine to coarse subangular mudstone fragments.			
		3.40	D		3.70	4.65		(MADE GROUND) medium dense? Grey clayey slightly sandy gravel. Gravel is fine to coarse subangular weak mudstone fragments.	4		
		4.20	SPT	N=21 (3,5/6,8,3,4)	4.20	4.15		(MADE GROUND) firm to stiff slightly sandy gravelly clay. Gravel is fine to coarse subangular mudstone and rare brick fragments.			
		4.30	D						5		
		4.50	D								
		4.50	ES						6		
		5.20 - 6.20	B		5.10	3.25		(MADE GROUND) medium dense? Grey clayey sandy gravel. Gravel is fine to coarse subangular weak mudstone fragments.			
		5.70	SPT	N=21 (9,11/6,5,5,5)					7		
		6.50	SPT	50 (5,6/50 for 215mm)	6.20	2.15		(MADE GROUND) loose to medium dense? Light brown slightly silty very sandy gravel. Gravel is fine to medium occasionally coarse subrounded mudstone and quartzite fragments and rare limestone cobbles. Very weak, locally extremely weak and weak, grey			
				6.50	1.85			8			
							slightly to moderately weathered calcareous MUDSTONE with occasional 5-10mm thick calcite veins. (BLUE LIAS FORMATION). Fractures are medium spaced (200, 350, 600) undulating smooth, dipping at 30-40°, no infill.	9			
								10			
Remarks Location CAT scanned and inspection pit hand excavated to 1.2m prior to drilling. Hole drilled by dynamic sampling to 7.00mbgl, then continued by rotary coring. Monitoring well installed to base of hole.											



				<h1 style="text-align: center;">Rotary Core Log</h1>				Borehole No. BH104			
Project Name: Watchet Harbour				Project No. 10501		Co-ords:		Sheet 2 of 2 Hole Type CP+RC			
Location: Somerset				Level: 8.35		Scale 1:50					
Client: Taunton Dean Bourough Council				Dates: 13/11/2018 - 14/11/2018		Logged By PW					
Well	Water Strikes	Depth (m)	Type /FI	Coring			Depth (m)	Level (m AOD)	Legend	Stratum Description	
				TCR	SCR	RQD					
		9.90 - 10.90	1	100	62	52	10.60	-2.25		Very weak, locally extremely weak and weak, grey slightly to moderately weathered calcareous MUDSTONE with occasional 5-10mm thick calcite veins. (BLUE LIAS FORMATION). Fractures are medium spaced (200, 350, 600) undulating smooth, dipping at 30-40°, no infill. Extremely weak, grey, calcareous MUDSTONE with rare calcite veins. Highly weathered and tending to very stiff clay. (BLUE LIAS FORMATION). No fractures visible	
		10.90 - 12.40		97	97	97					
							12.35 12.40	-4.00 -4.05		Weak to medium strong grey LIMESTONE. (BLUE LIAS FORMATION). End of Borehole at 12.400m	
Remarks Location CAT scanned and inspection pit hand excavated to 1.2m prior to drilling. Hole drilled by dynamic sampling to 7.00mbgl, then continued by rotary coring. Monitoring well installed to base of hole.											

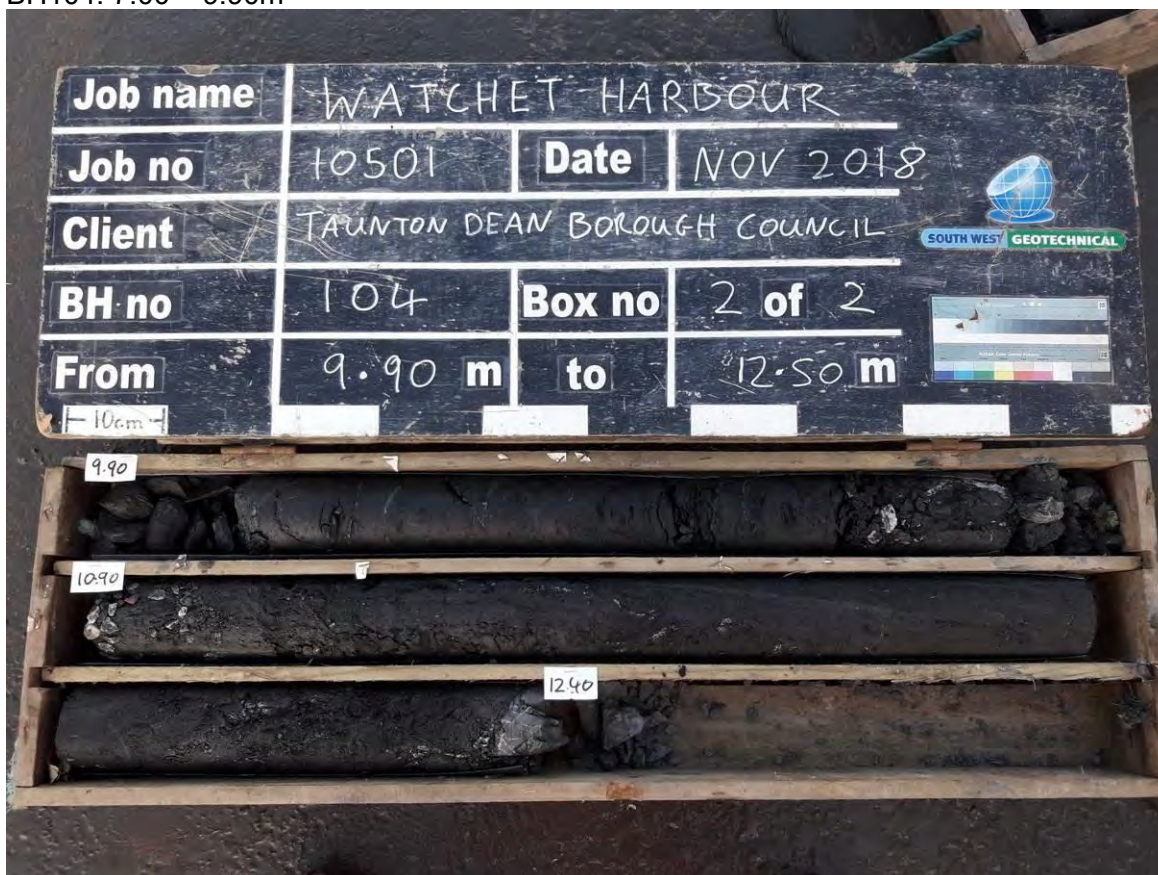





Pick Everard





BH104: 7.00 – 9.90m





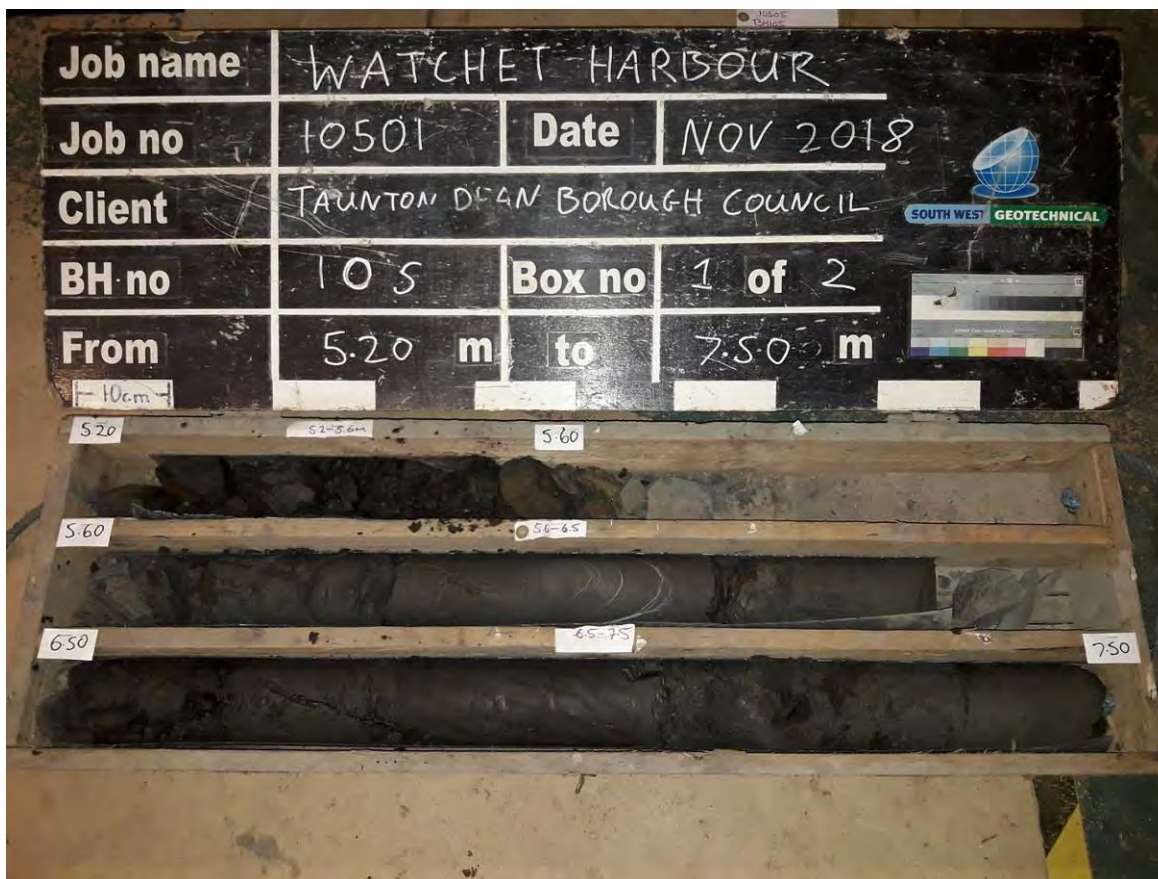
BH104: 9.90 – 12.50m

					<h1 style="text-align: center;">Borehole Log</h1>					Borehole No. BH105 Sheet 1 of 2	
Project Name: Watchet Harbour					Project No. 10501		Co-ords:		Hole Type CP+RC		
Location: Somerset					Level: 8.50		Scale 1:50			Logged By PW	
Client: Taunton Dean Bourough Council					Dates: 15/11/2018						

Well	Water Strikes	Sample and In Situ Testing				Depth (m)	Level (m AOD)	Legend	Stratum Description	
		Depth (m)	Type	Results						
		0.20 0.30				8.30 8.20		Concrete with 1 layer of 6mm rebar.		
		0.50 0.50	D ES				0.70 7.80	(MADE GROUND) compact red brown sandy gravel-sub-base material (MADE GROUND) brown slightly sandy gravelly clay with occasional brick fragments. (MADE GROUND) Grey sandy slightly gravelly silt.	1	
		1.00 1.00 1.20	D ES SPT	50 (25 for 85mm/50 for 80mm)			1.20 7.30	(MADE GROUND) pale yellow very lime mortar.		
						1.80 6.70		(MADE GROUND) Medium brown and grey brown slightly sandy slightly gravelly clay with occasional brick fragments.	2	
		2.20 2.20	D SPT	N=5 (1,1/2,1,1,1)			2.20 6.30 2.40 6.10 2.60 5.90	(MADE GROUND) Soft light brown slightly gravelly clay. Gravel is fine to coarse subangular mudstone and limestone fragments. (MADE GROUND) Soft grey slightly sandy slightly gravelly clay. (MADE GROUND) Soft red brown slightly gravelly clay with low cobble content. Gravel and cobbles are subangular mudstone fragments.	3	
		3.00 3.30 - 4.80	D B				3.30 5.20	(MADE GROUND) medium dense grey clayey sandy gravel with medium cobble content. Gravel is fine to coarse subangular mudstone fragments.	4	
		3.70	SPT	N=15 (6,5/3,6,3,3)				4.85-4.90 Layer of sandy subrounded gravel.		
		5.05	SPT	50 (3,11/50 for 15mm)			5.05 3.45	(MADE GROUND/ALLUVIUM?) Medium brown sandy	5	
		5.20 - 5.60	50	100	16	0	5.20 3.30	slightly gravelly clay. Gravel is fine to medium subrounded mudstone and quartzite fragments.		
		5.60 - 6.50		100	78	64		Very weak, locally extremely weak, dark grey, moderately locally highly weathered, calcareous MUDSTONE. (BLUE LIAS FORMATION).	6	
	6.50 - 7.50	5	100	80	80		Fractures are closely to medium spaced (160, 200, 340), planar smooth, dipping at 30-40° (J1) and 65-70° (J2), no infill	7		
	7.50 - 9.00		100	93	65	7.50 1.00 7.90 0.60	Strong, pale, grey, fresh LIMESTONE with 1-30mm thick calcite veins. (BLUE LIAS FORMATION).	8		
		50					No fractures.			
	9.00 - 10.50	4	100	70	60		Very weak, locally extremely weak, dark grey, moderately locally highly weathered, calcareous MUDSTONE. (BLUE LIAS FORMATION).	9		
							Fractures are closely to medium spaced (120, 300, 400), planar smooth, dipping at 30-40° (J1) and 65-70° (J2), no infill	10		

Remarks Location CAT scanned and inspection pit hand excavated to 1.2m prior to drilling. Hole drilled by dynamic sampling to 5.20mbgl, then continued by rotary coring. Monitoring well installed to base of hole.		
--	--	---

				<h1 style="text-align: center;">Rotary Core Log</h1>				Borehole No. BH105			
Project Name: Watchet Harbour				Project No. 10501		Co-ords:		Sheet 2 of 2 Hole Type CP+RC			
Location: Somerset				Level: 8.50		Scale 1:50					
Client: Taunton Dean Bourough Council				Dates: 15/11/2018 - 16/11/2018		Logged By PW					
Well	Water Strikes	Depth (m)	Type /FI	Coring			Depth (m)	Level (m AOD)	Legend	Stratum Description	
				TCR	SCR	RQD					
							10.50	-2.00		Very weak, locally extremely weak, dark grey, moderately locally highly weathered, calcareous MUDSTONE. (BLUE LIAS FORMATION). Fractures are closely to medium spaced (120, 300, 400), planar smooth, dipping at 30-40° (J1) and 65-70° (J2), no infill End of Borehole at 10.500m	11
											12
											13
											14
											15
											16
											17
											18
											19
											20
Remarks Location CAT scanned and inspection pit hand excavated to 1.2m prior to drilling. Hole drilled by dynamic sampling to 5.20mbgl, then continued by rotary coring. Monitoring well installed to base of hole.											



BH105: 5.20 – 7.50m



BH105: 7.50 – 10.50m

Appendix E

Plate Load Test Results



Transmittal Note

South West Geotechnical Ltd
Unit 3 Brooklands,
Howden Road,
Tiverton,
Devon
EX16 5HW

Job No:	10501	Date Received:	09/11/18
Job Name:	Watchet Harbour	Date Sent:	12/11/18
Client Name:	Internal Job	Transmittal Number:	T4039
Client Job No:	-	Senders Initials:	DT
Client Address	For client address details, please refer to the final report.		

Ref.	Test Detail	No. of Tests / Report No.
PLOAD	BS1377: Part 9: 1990: Clause 4.1 - Determination of Vertical Deformation and Strength Characteristics of Soil by the Plate Loading Test - UKAS Accredited	2

Approved Signatories:

Nick Worthington-Williams (Laboratory Quality Manager), Dan Ayre (Deputy Quality Manager)

David Trowbridge (Laboratory Manager)

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	Report on the Determination of Vertical Deformation and Strength Characteristics of Soil to BS1377:Part 9 CL 4.1		Project No.	10501	
			Test Location ID	PL01	
Project Name	Watchet Harbour		Depth, m	0.20	
Soil Description	Mixed Fill		Reaction Load / Kentledge	4 Tonne	
Client Job No.	-	Date Tested	09/11/2018	Easting	-
Client	Internal Job		Northing	-	
Test Location	Logged by engineer		Weather	Dry	

Settlement vs Load



Settlement vs Time



Settlement vs Time (Logarithmic)



Settlement vs Time (Individual Stages)




Plate Diameter (mm)	450	Maximum Applied Pressure (kPa)	207.9	Maximum Deformation (mm)	12.09
----------------------------	-----	---------------------------------------	-------	---------------------------------	-------

In-situ Density (Mg/m³) (If requested)	-	Moisture Content (%) (If requested)	-
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Notes:			
Modulus of subgrade reaction Stage 1 - 10732 Stage 2 - 9059 Stage 3 - 9814 Stage 4 - 10499 Stage 5 - 10709			
Page No.	1	Date	Approved
KL039 Plate Load (Incremental)		18/12/2018	David Trowbridge - Laboratory Manager



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	Report on the Determination of Vertical Deformation and Strength Characteristics of Soil to BS1377:Part 9 CL 4.1			Project No.	10501
				Test Location ID	PL02
Project Name	Watchet Harbour			Depth, m	0.20
Soil Description	Mixed Fill			Reaction Load / Kentledge	4 Tonnes
Client Job No.	-	Date Tested	09/11/2018	Easting	-
Client	Internal Job			Northing	-
Test Location	Logged by engineer			Weather	Dry

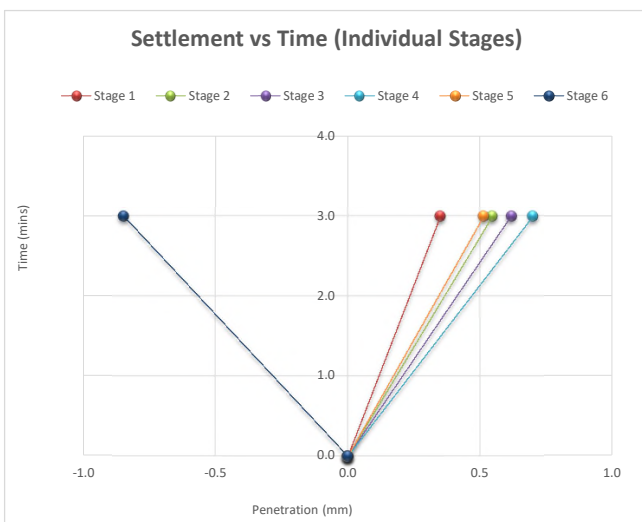
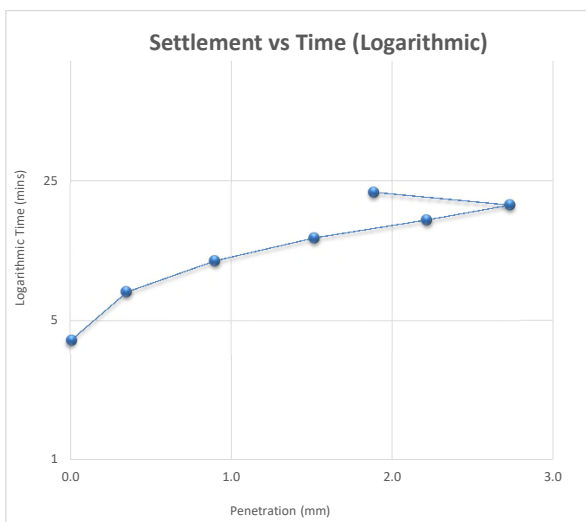
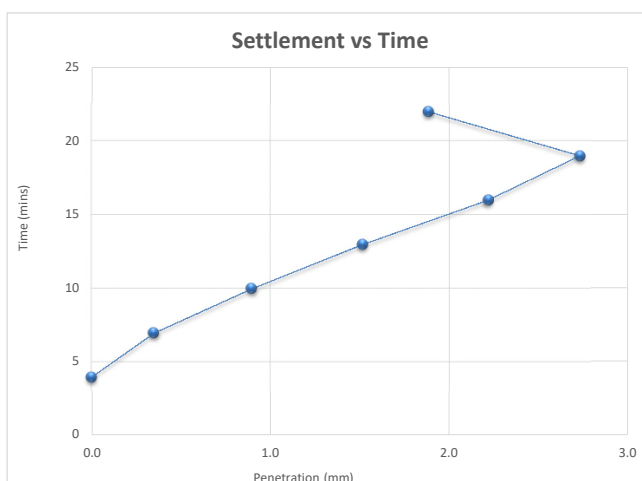
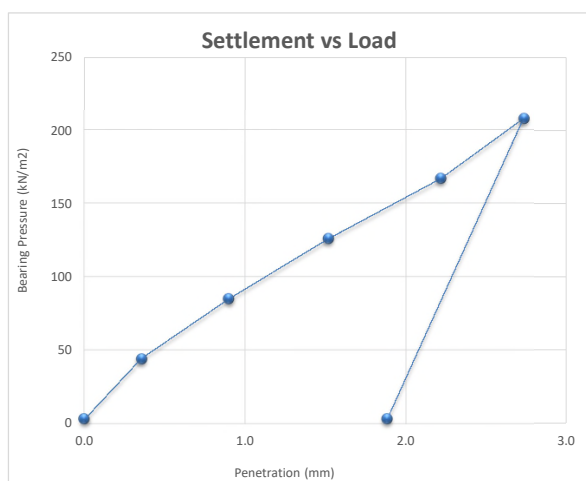



Plate Diameter (mm)	450	Maximum Applied Pressure (kPa)	207.9	Maximum Deformation (mm)	2.73
In-situ Density (Mg/m3) (If requested)	-	Moisture Content (%) (If requested)	-	<div> 8260 Accredited to ISO/IEC 17025:2005</div>	
Notes: Modulus of subgrade reaction Stage 1 - 79010 Stage 2 - 59239 Stage 3 - 51926 Stage 4 - 47008 Stage 5 - 47497					
Page No.	2	Date	Approved		
KL039 Plate Load (Incremental)		18/12/2018	David Trowbridge - Laboratory Manager		

Appendix F

Geotechnical Laboratory Test Results



Summary of Classification Test Results

Unit 3 Brooklands,
Howden Road,
Tiverton,
Devon
EX16 5HW



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Project No.	Project Name
10501	Watchet Harbour
Client Job No.	Client
10501	Internal

Hole No.	Sample				Soil Description	mc	Passing 425µm	LL	PL	PI	Particle density	Remarks
	Type	Top	Base	Ref		CI.3.2			CI5.3	CI5.4		
						%	%	%	%	%	Mg/m3	
BH101	D	1.50		-	Reddish brown and greenish grey very sandy clayey silty GRAVEL	14	35 - Sieved	32 - 1pt	22	10	-	
BH101	B	2.70	3.60	-	Grey and reddish brown sandy silty GRAVEL	7.3	-	-	-	-	-	
BH101	D	4.50		-	Greenish grey and brown sandy clayey GRAVEL	21	29 - Sieved	50 - 1pt	23	27	-	
BH101	D	5.50		-	Brown and greenish grey sandy clayey GRAVEL	21	25 - Sieved	45 - 1pt	22	23	-	
BH102	B	1.40	2.70	-	Black silty very sandy GRAVEL	24	-	-	-	-	-	
BH102	D	3.60		-	Dark brown silty very sandy GRAVEL	16	29 - Sieved	31 - 1pt	19	12	-	
BH102	B	5.30	5.90	-	Brown sandy clayey GRAVEL	13	-	-	-	-	-	
BH103	B	2.80	3.10	-	Reddish brown and brown slightly gravelly sandy silty CLAY	12	-	-	-	-	-	
BH103	B	4.60	5.70	-	Grey sandy clayey GRAVEL	14	-	-	-	-	-	
BH104	D	1.80		-	Dark brown sandy silty GRAVEL	12	32 - Sieved	31 - 1pt	19	12	-	

Preparation Clauses: Particle Density (BS1377:Part 1: 1990: CL7.4.4) Atterberg Limits (BS1377:Part 1: 1990: CL7.4.3) Moisture Content (BS1377: Part 1: 1990: CL7.3.3 & 7.4.2)

Key		Date	Approved By	Page No.	1
Atterberg Limits BS1377-2:1990 4pt cone (CL.4.3) unless : 1pt - single point test (CL.4.4) 4.2.3 - Natural 4.2.4 - Sieved Moisture Content (mc) %		18/12/2018	Nick W-W - QM	KL001R Index Summary	
Particle density BS1377-2:1990 sp - small pyknometer CL.8.3 gj - gas jar CL.8.2					



Summary of Classification Test Results

Unit 3 Brooklands,
Howden Road,
Tiverton,
Devon
EX16 5HW



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Project No.	Project Name
10501	Watchet Harbour
Client Job No.	Client
10501	Internal

Hole No.	Sample				Soil Description	mc	Passing 425µm	LL	PL	PI	Particle density	Remarks
	Type	Top	Base	Ref		CI.3.2			CI5.3	CI5.4		
						%	%	%	%	%	Mg/m3	
BH104	D	3.40		-	Reddish brown very sandy very clayey GRAVEL	16	48 - Sieved	31 - 1pt	18	13	-	
BH104	D	4.30		-	Grey very sandy silty GRAVEL	12	33 - Sieved	34 - 1pt	20	14	-	
BH104	B	5.20	6.20	-	Grey sandy clayey GRAVEL	13	-	-	-	-	-	
BH105	D	2.20		-	Greenish brown slightly sandy slightly gravelly CLAY	26	69 - Sieved	50 - 1pt	23	27	-	
BH105	D	3.00		-	Reddish brown and greenish grey slightly sandy gravelly CLAY	16	43 - Sieved	34 - 1pt	18	16	-	
BH105	B	3.30	4.80	-	Grey sandy clayey GRAVEL	13	-	-	-	-	-	
						-	-	-	-	-	-	
						-	-	-	-	-	-	
						-	-	-	-	-	-	
						-	-	-	-	-	-	

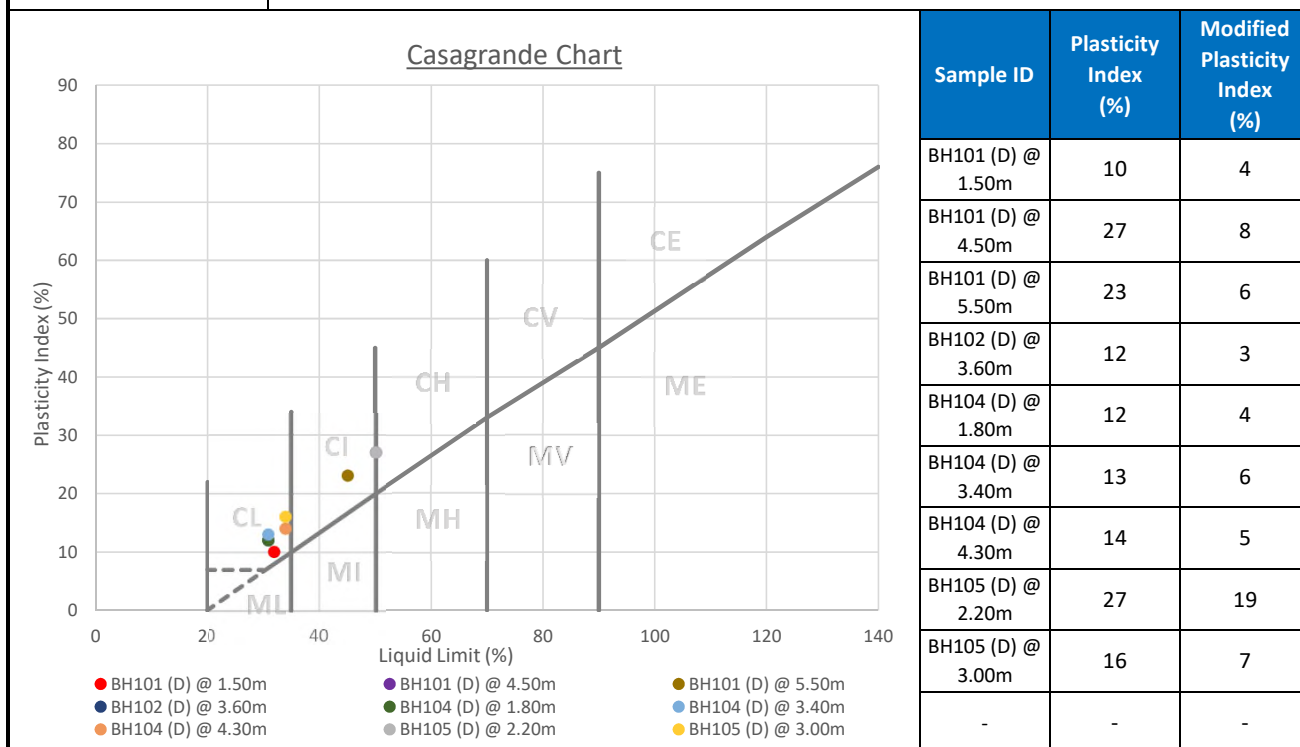
Preparation Clauses: Particle Density (BS1377:Part 1: 1990: CL7.4.4) Atterberg Limits (BS1377:Part 1: 1990: CL7.4.3) Moisture Content (BS1377: Part 1: 1990: CL7.3.3 & 7.4.2)

Key						Date	Approved By	Page No.	2
Atterberg Limits BS1377-2:1990 4pt cone (CL.4.3) unless : 1pt - single point test (CL.4.4) 4.2.3 - Natural 4.2.4 - Sieved Moisture Content (mc) %						18/12/2018	Nick W-W - QM	KL001R Index Summary	
Particle density BS1377-2:1990 sp - small pyknometer CL.8.3 gj - gas jar CL.8.2									

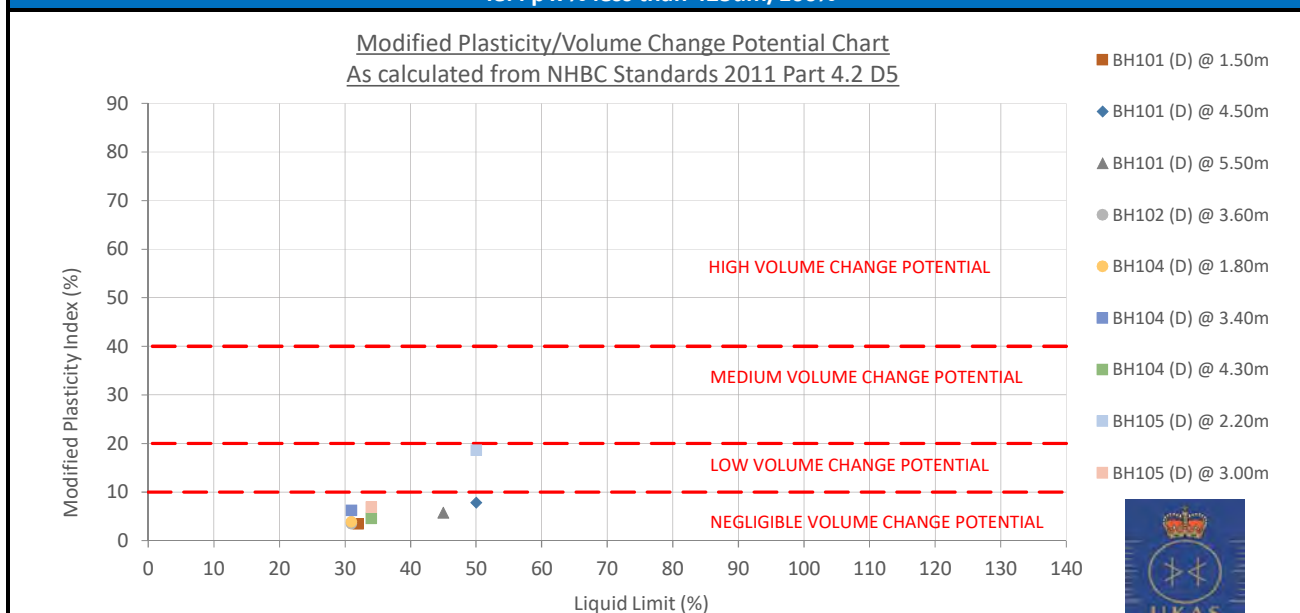
Graphical Summary of Atterberg Test Results

Unit 3 Brooklands,
Howden Road,
Tiverton,
Devon
EX16 5HW


Project No.	Project Name
10501	Watchet Harbour
Client Job No.	Client
-	Internal Job

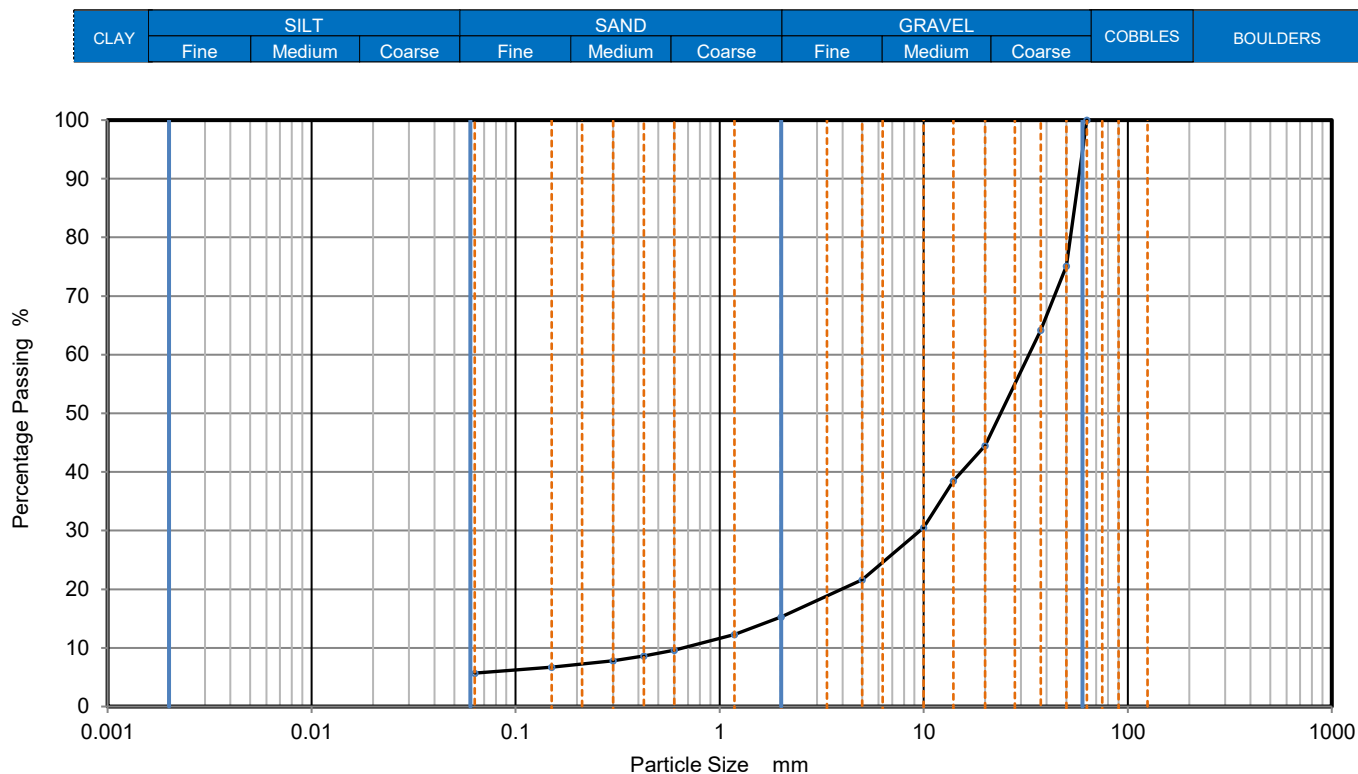


The Modified Plasticity Index (I_p) is defined as the Plasticity Index (I_p) of the soil multiplied by the percentage of particles less than 425 μ m.
ie. $I_p \times \% \text{ less than } 425\mu\text{m} / 100\%$



KL001a Index Graphical Summary	Approved By	Date	Page No.
	Nick W-Williams - Quality Manager	10/12/2018 17:12	1

	Particle Size Distribution BS1377:Part 2:1990, clause 9.2		Project No.		10501	
			Borehole/Pit No.		BH101	
Project Name		Watchet Harbour		Sample No.		-
Soil Description		Grey and reddish brown sandy silty GRAVEL		Depth, m		2.70 - 3.60
Client Job No.		10501		Specimen Depth		2.70 m
Client		Internal		Sample Type		B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	-	-	-
75	-	-	-
63	100	-	-
50	75		
37.5	64		
20	45		
14	39		
10	31		
5	22		
2	15		
1.18	12		
0.6	10		
0.425	9		
0.3	8		
0.15	7		
0.063	6		

Sedimentation pre-treatment
N/A

Dry Mass of sample, g	4550
-----------------------	------

Sample Proportions	% dry mass
Very coarse	0
Gravel	85
Sand	10
Fines <0.063mm	6


Grading Analysis		
D100	mm	63
D60	mm	32.8
D30	mm	9.65
D10	mm	0.665
Uniformity Coefficient		49
Curvature Coefficient		4.3

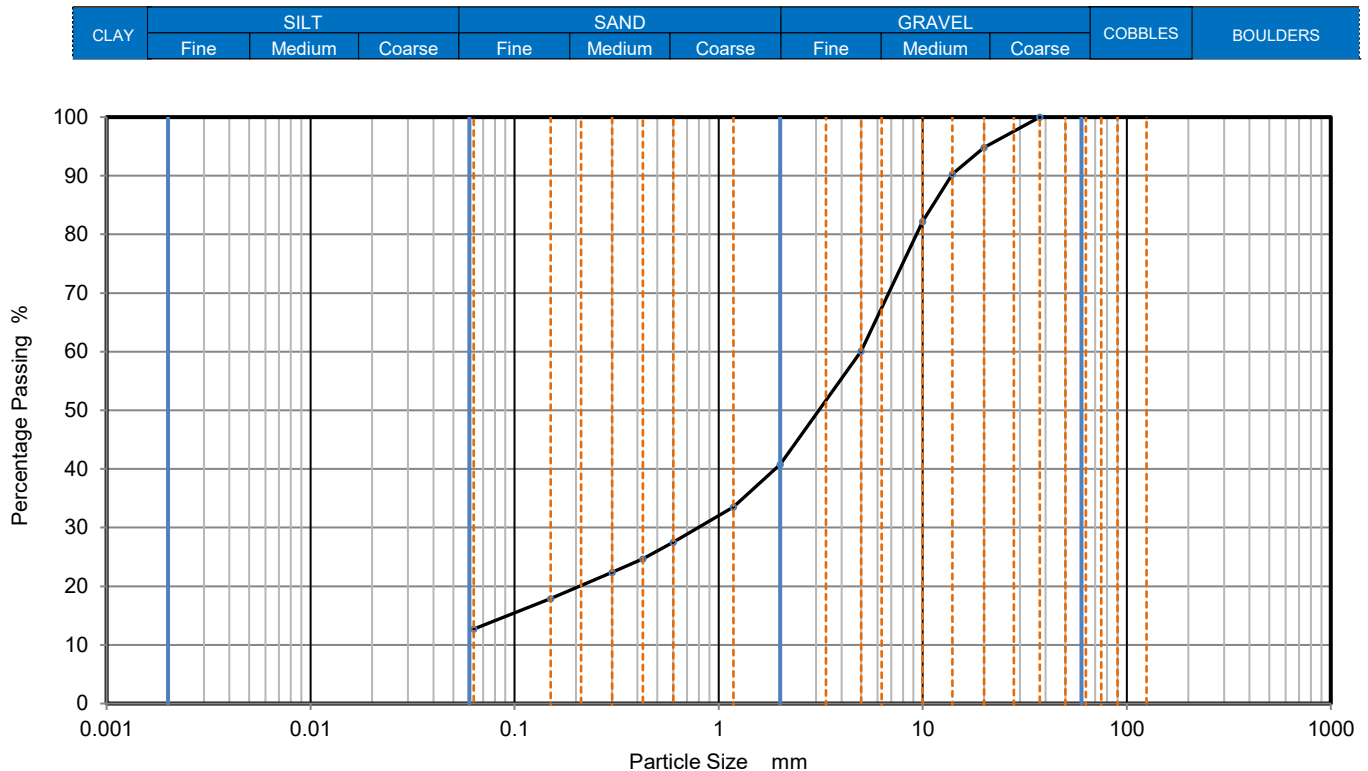
Remarks
Preparation and testing in accordance with BS1377 - Deviation to standard as insufficient material provided in order to meet the minimum mass requirement



Page No.	1	Date	Approved
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	Particle Size Distribution BS1377:Part 2:1990, clause 9.2		Project No.		10501	
			Borehole/Pit No.		BH102	
Project Name		Watchet Harbour		Sample No.		-
Soil Description		Black silty very sandy GRAVEL		Depth, m		1.40 - 2.70
Client Job No.		10501		Specimen Depth		1.40 m
Client		Internal		Sample Type		B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	-	-	-
75	-	-	-
63	-	-	-
50	-		
37.5	100		
20	95		
14	90		
10	82		
5	60		
2	41		
1.18	34		
0.6	28		
0.425	25		
0.3	22		
0.15	18		
0.063	13		

Sedimentation pre-treatment
N/A

Dry Mass of sample, g	1064
-----------------------	------

Sample Proportions	% dry mass
Very coarse	0
Gravel	59
Sand	28
Fines <0.063mm	13


Grading Analysis		
D100	mm	37.5
D60	mm	4.99
D30	mm	0.795
D10	mm	
Uniformity Coefficient		
Curvature Coefficient		

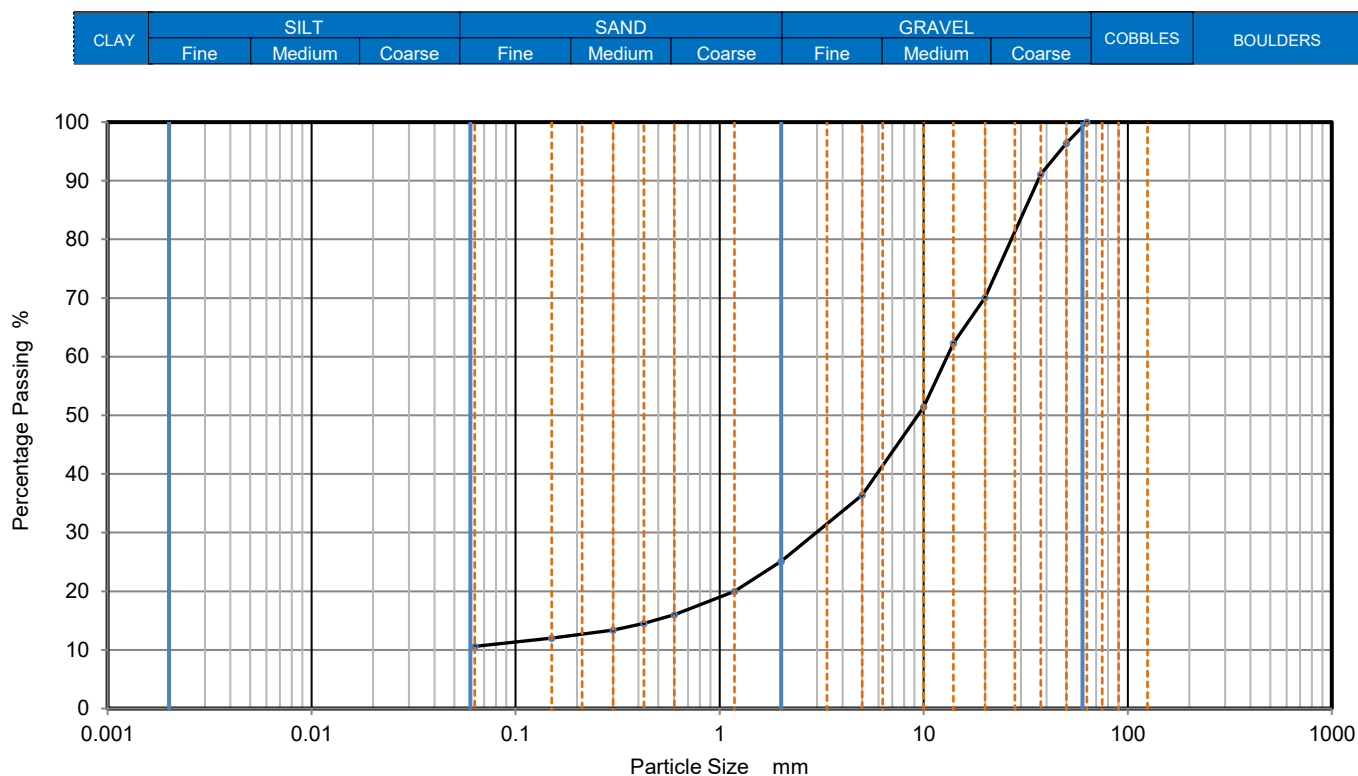
Remarks
Preparation and testing in accordance with BS1377: Part 1: 1990 CL7.3 & 7.4.5



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	Particle Size Distribution BS1377:Part 2:1990, clause 9.2		Project No.		10501	
			Borehole/Pit No.		BH102	
Project Name		Watchet Harbour		Sample No.		-
Soil Description		Brown sandy clayey GRAVEL		Depth, m		5.30 - 5.90
Client Job No.		10501		Specimen Depth		5.30 m
Client		Internal		Sample Type		B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	-	-	-
75	-	-	-
63	100	-	-
50	96		
37.5	91		
20	70		
14	62		
10	51		
5	36		
2	25		
1.18	20		
0.6	16		
0.425	15		
0.3	13		
0.15	12		
0.063	11		

Sedimentation pre-treatment
N/A

Dry Mass of sample, g	5089
-----------------------	------

Sample Proportions	% dry mass
Very coarse	0
Gravel	75
Sand	15
Fines <0.063mm	11


Grading Analysis		
D100	mm	63
D60	mm	13
D30	mm	2.97
D10	mm	
Uniformity Coefficient		
Curvature Coefficient		

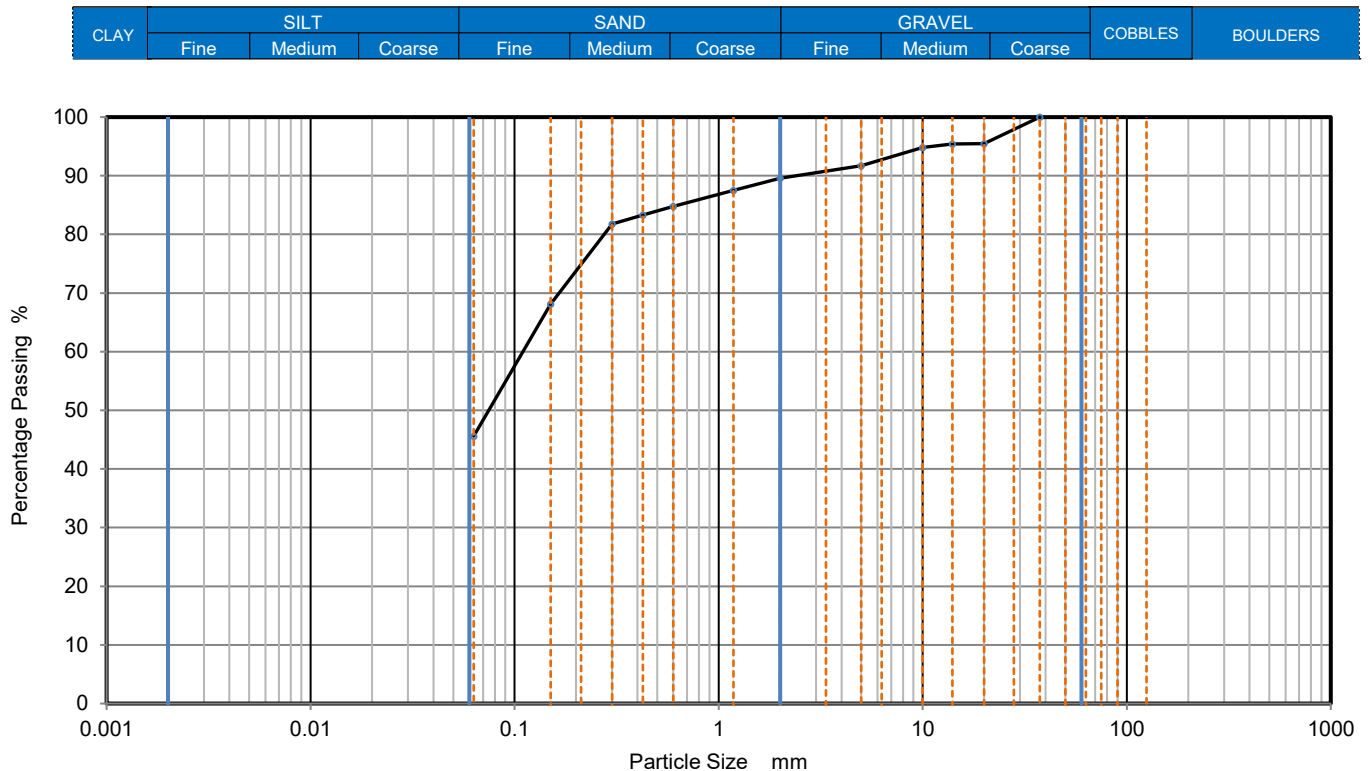
Remarks
Preparation and testing in accordance with BS1377: Part 1: 1990 CL7.3 & 7.4.5



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	Particle Size Distribution BS1377:Part 2:1990, clause 9.2		Project No.		10501	
			Borehole/Pit No.		BH103	
Project Name		Watchet Harbour		Sample No.		-
Soil Description		Reddish brown and brown slightly gravelly sandy silty CLAY		Depth, m		2.80 - 3.10
Client Job No.		10501		Specimen Depth		2.80 m
Client		Internal		Sample Type		B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	-	-	-
75	-	-	-
63	-	-	-
50	-		
37.5	100		
20	96		
14	95		
10	95		
5	92		
2	90		
1.18	88		
0.6	85		
0.425	83		
0.3	82		
0.15	68		
0.063	46		

Sedimentation pre-treatment
N/A

Dry Mass of sample, g	2023
-----------------------	------

Sample Proportions	% dry mass
Very coarse	0
Gravel	10
Sand	44
Fines <0.063mm	46


Grading Analysis		
D100	mm	37.5
D60	mm	0.11
D30	mm	
D10	mm	
Uniformity Coefficient		
Curvature Coefficient		

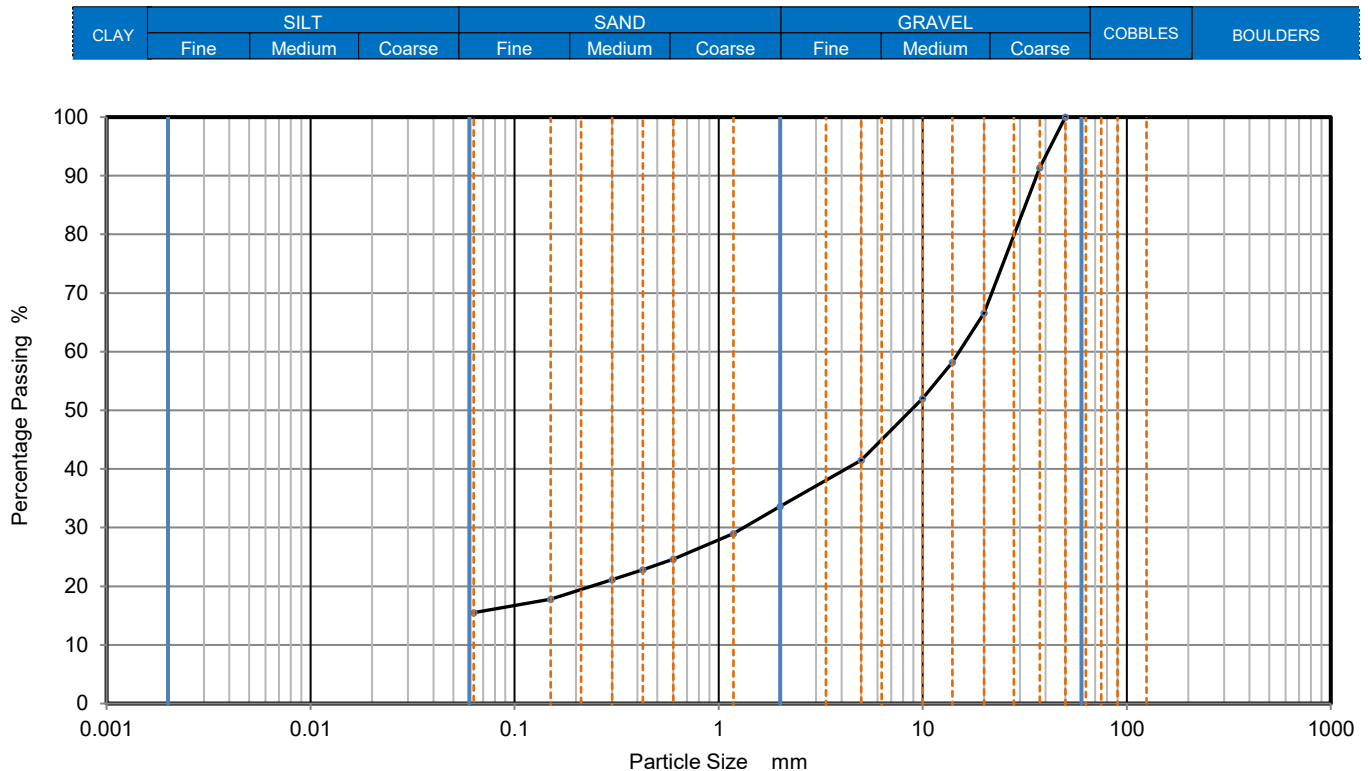
Remarks
Preparation and testing in accordance with BS1377: Part 1: 1990 CL7.3 & 7.4.5



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	Particle Size Distribution BS1377:Part 2:1990, clause 9.2		Project No.		10501	
			Borehole/Pit No.		BH103	
Project Name		Watchet Harbour		Sample No.		-
Soil Description		Grey sandy clayey GRAVEL		Depth, m		4.60 - 5.70
Client Job No.		10501		Specimen Depth		4.60 m
Client		Internal		Sample Type		B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	-	-	-
75	-	-	-
63	-	-	-
50	100		
37.5	91		
20	67		
14	58		
10	52		
5	42		
2	34		
1.18	29		
0.6	25		
0.425	23		
0.3	21		
0.15	18		
0.063	16		

Sedimentation pre-treatment
N/A

Dry Mass of sample, g	6216
-----------------------	------

Sample Proportions	% dry mass
Very coarse	0
Gravel	66
Sand	18
Fines <0.063mm	16


Grading Analysis		
D100	mm	50
D60	mm	15.1
D30	mm	1.32
D10	mm	
Uniformity Coefficient		
Curvature Coefficient		

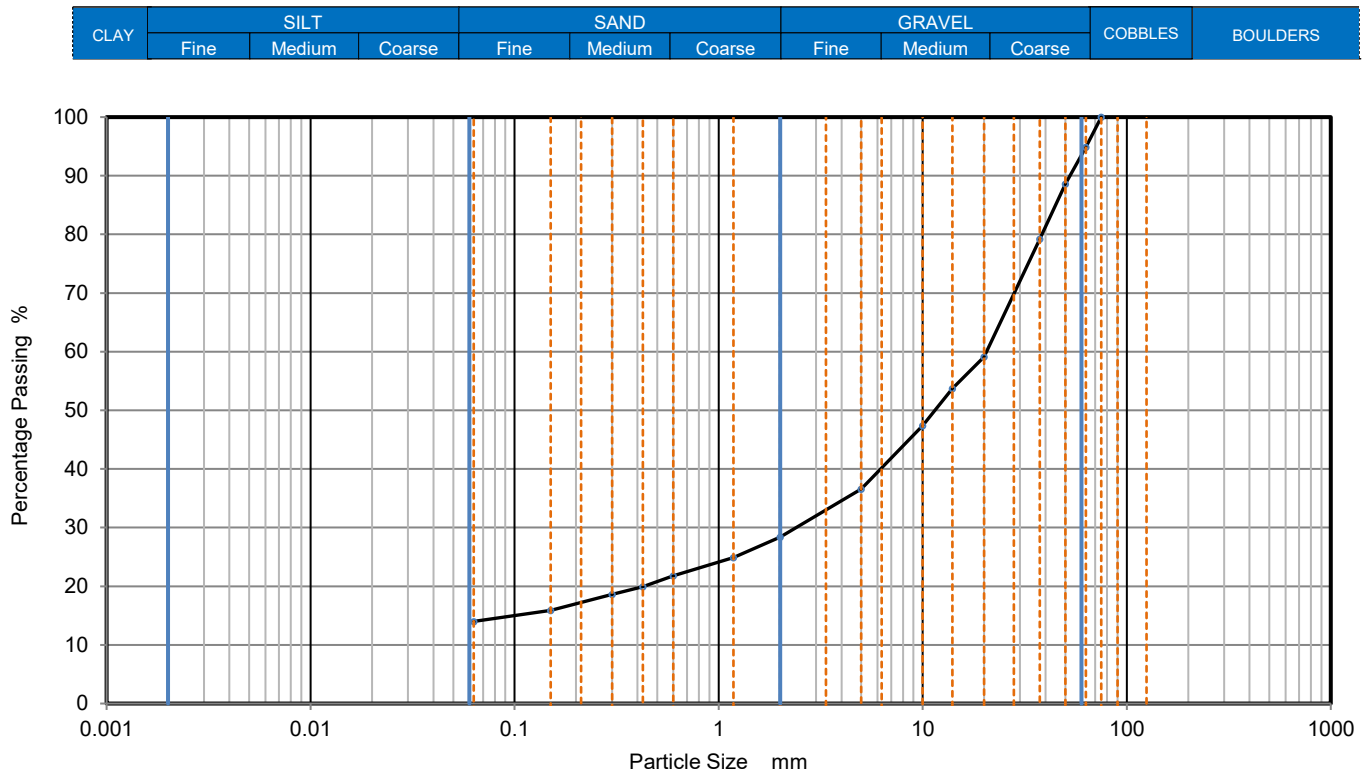
Remarks
Preparation and testing in accordance with BS1377: Part 1: 1990 CL7.3 & 7.4.5



Page No.	5	Date	Approved
Sheet ID: KL002R PSD		10/12/2018 16:58	Nick W-W - QM

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	Particle Size Distribution BS1377:Part 2:1990, clause 9.2		Project No.	10501		
			Borehole/Pit No.	BH104		
Project Name	Watchet Harbour		Sample No.	-		
Soil Description	Grey sandy clayey GRAVEL		Depth, m	5.20	-	6.20
Client Job No.	10501	Specimen Depth	5.20	m	Sample Type	B
Client	Internal					



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	-	-	-
75	100	-	-
63	95	-	-
50	89		
37.5	79		
20	59		
14	54		
10	47		
5	37		
2	28		
1.18	25		
0.6	22		
0.425	20		
0.3	19		
0.15	16		
0.063	14		

Sedimentation pre-treatment
N/A

Dry Mass of sample, g	9566
-----------------------	------

Sample Proportions	% dry mass
Very coarse	5
Gravel	67
Sand	14
Fines <0.063mm	14


Grading Analysis		
D100	mm	75
D60	mm	20.5
D30	mm	2.4
D10	mm	
Uniformity Coefficient		
Curvature Coefficient		

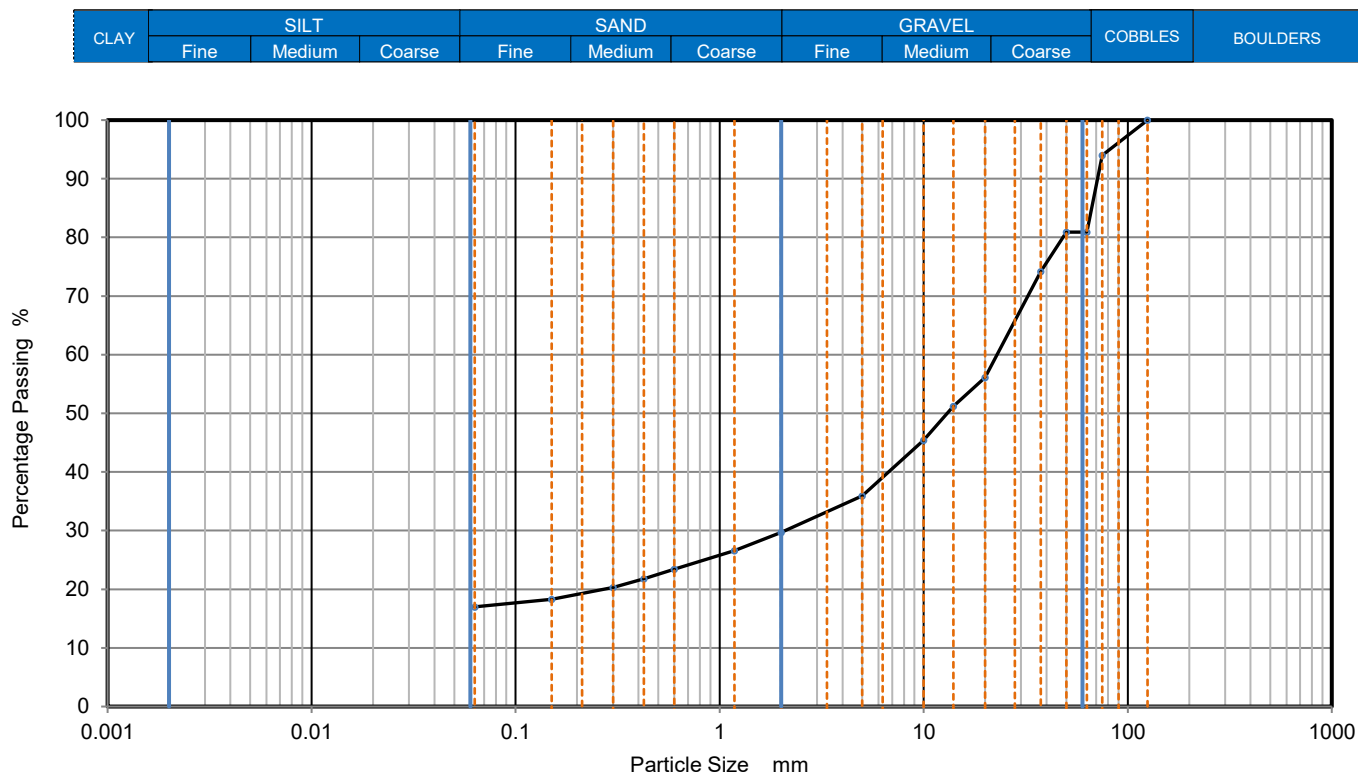
Remarks
Preparation and testing in accordance with BS1377 - Deviation to standard as insufficient material provided in order to meet the minimum mass requirement



Page No.	6	Date	Approved
Sheet ID: KL002R PSD		10/12/2018 16:58	Nick W-W - QM

8260
Accredited to
ISO/IEC
17025:2005

	Particle Size Distribution BS1377:Part 2:1990, clause 9.2		Project No.		10501	
			Borehole/Pit No.		BH105	
Project Name		Watchet Harbour		Sample No.		-
Soil Description		Grey sandy clayey GRAVEL		Depth, m		3.30 - 4.80
Client Job No.		10501		Specimen Depth		3.30 m
Client		Internal		Sample Type		B



Sieving		Sedimentation	
Particle Size mm	% Passing	Particle Size mm	% Passing
125	100	-	-
75	94	-	-
63	81	-	-
50	81		
37.5	74		
20	56		
14	51		
10	45		
5	36		
2	30		
1.18	27		
0.6	23		
0.425	22		
0.3	20		
0.15	18		
0.063	17		

Sedimentation pre-treatment
N/A

Dry Mass of sample, g	7873
-----------------------	------

Sample Proportions	% dry mass
Very coarse	19
Gravel	51
Sand	13
Fines <0.063mm	17

Grading Analysis		
D100	mm	125
D60	mm	22.9
D30	mm	2.09
D10	mm	
Uniformity Coefficient		
Curvature Coefficient		

Remarks
Preparation and testing in accordance with BS1377 - Deviation to standard as insufficient material provided in order to meet the minimum mass requirement



Page No.	7	Date	Approved
Sheet ID: KL002R PSD		10/12/2018 16:58	Nick W-W - QM

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Determination of Shear Strength using the
Small Direct Shearbox Apparatus

Unit 3 Brooklands,
Howden Road,
Tiverton,
Devon
EX16 5HW

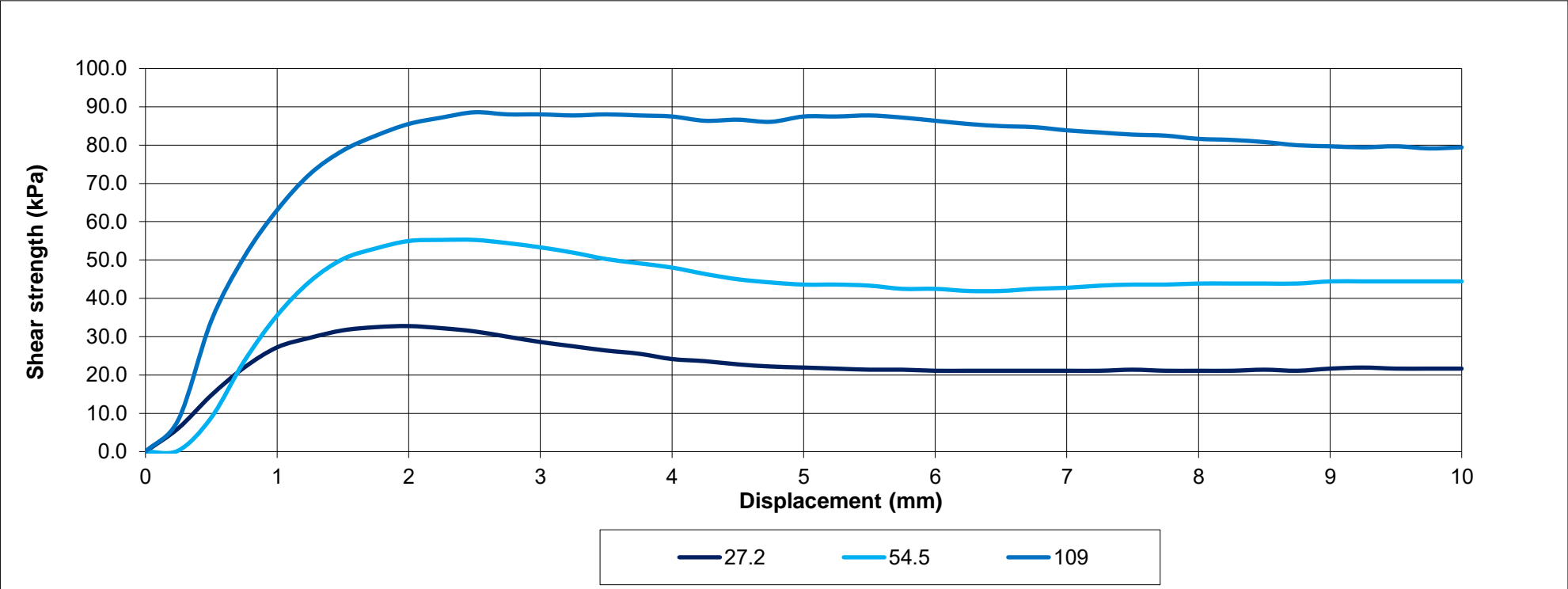
Project Name	Watchet Harbour	Project No.	10501
Client:	Pick Everard	Borehole / Pit No.	BH102
Soil Description	Black silty very sandy GRAVEL	Client Job No:	-
Specimen Description	Black silty SAND	Depth (m)	1.40 - 2.70
Test Method	Tests carried out in accordance with Clause 4 of BS1377: 1990: Part 7: CL 4.5.4 (Single Stage) using the fraction passing a 2.0mm sieve	Sample No.	-
Sample Type	Bulk Sample	Date of test	03/12/2018

Preparation Details	Test prepared in accordance with BS1377:1990:Part 7: CL4.4.3.5	Assumed Particle Density (Mg/m3)	2.65
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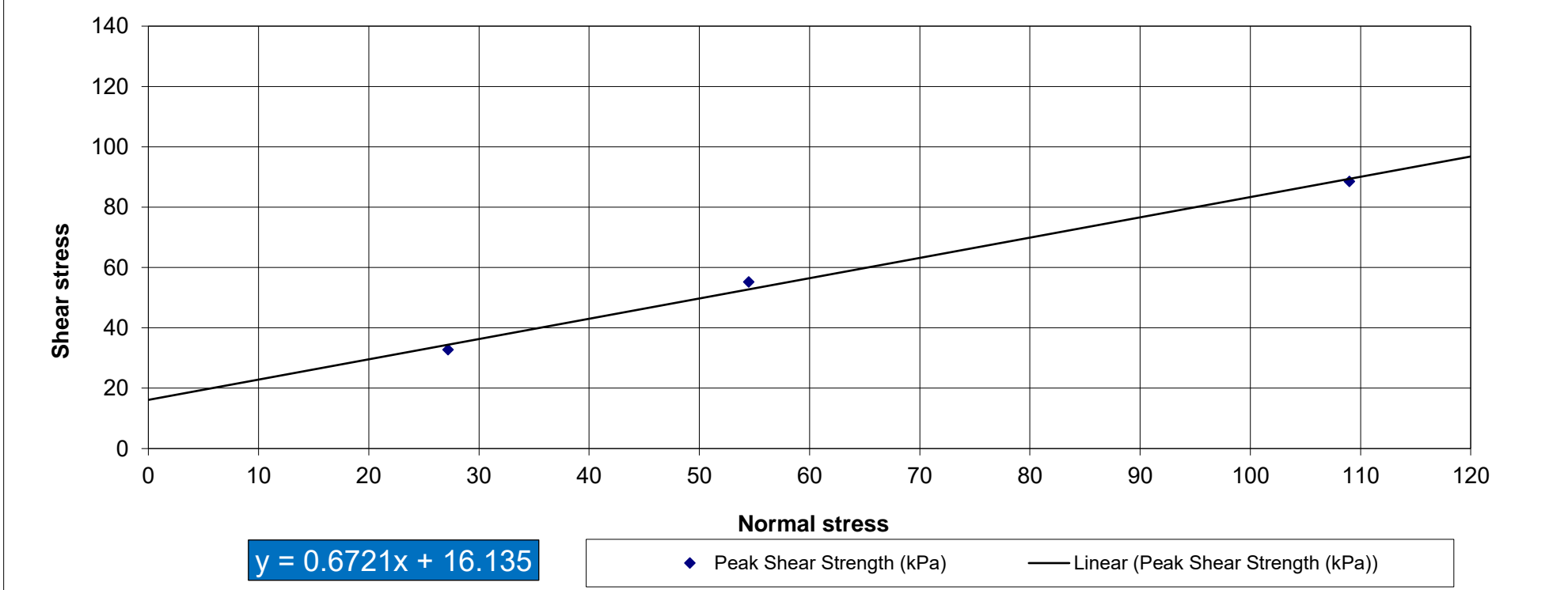
Rate of displacement (mm/min)	Test Dry or Submerged	Load Stage (kPa)	Initial Moisture Content %	Initial Height (mm)	Initial Bulk Density (Mg/m3)	Initial Dry Density (Mg/m3)	Specimen Width (mm)	Specimen Length (mm)	Consolidated Height (mm)	Peak Shear Strength (kPa)	Horizontal Displacement At Peak
0.10861	Submerged	27.2	28	20.10	1.34	1.05	60.01	60.02	19.92	33	2.00mm
		54.5		20.10	1.33	1.04			19.85	55	2.25mm
		109		20.11	1.32	1.04			19.81	89	2.50mm

Angle of friction (Peak) °	34	Peak Cohesion (kPa)	16	Angle of friction (Residual) °	-	Residual Cohesion (kPa)	-
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Shear stress versus Horizontal Displacement



Maximum shear stress versus Normal Applied Stress



Accredited to
ISO/IEC
17025:2005

Remarks:

Approved by

Dan Ayre - Deputy Quality Manager

Date Approved

06/12/2018 09:41



Summary of Rock Testing

ISRM: 1981: Part 2 Suggested Methods - Uniaxial Compressive Strength of Rock materials

Unit 3 Brooklands,
Howden Road,
Tiverton,
Devon EX16 5HW

Date of test	03/12/18
Project Name	Watchet Harbour
Project No.	10501
Client	Internal Job
Client Job No.	-

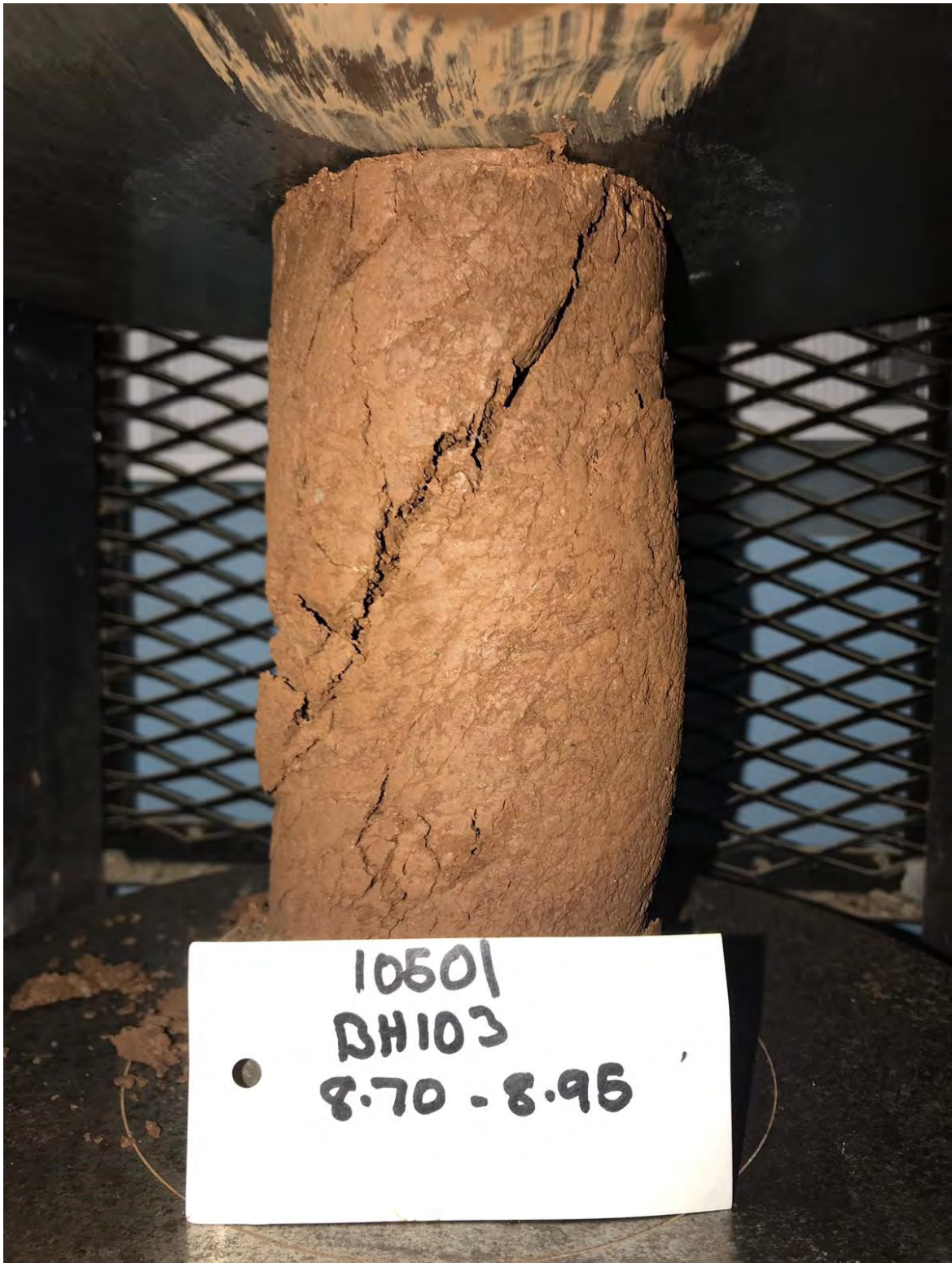
Sample Details				Density			Uniaxial Compressive Strength				
Borehole No.	Sample Reference	Depth (m)	Description	Water Content (%)	Bulk (Mg/m ³)	Dry (Mg/m ³)	Diameter (mm)	Height (mm)	H/D Ratio	Load at Failure (kN)	UCS (Mpa)
BH101		10.60 - 11.00	Brown MUDSTONE	3.9	2.55	2.46	79.08	238.00	3.0	18.5	3.8
BH102		8.00 - 8.30	Brown MUDSTONE	5.1	2.53	2.40	79.48	197.00	2.5	25.7	5.2
BH103		8.70 - 8.95	Brown MUDSTONE	13	2.26	2.00	76.66	187.67	2.4	3.5	0.8
BH105		7.50 - 7.90	Grey with white veins LIMESTONE	0.75	2.71	2.69	79.25	198.00	2.5	309.3	62.7

KL037 - Uniaxial Compressive Strength of Rock	Remarks	Approved By	Date	Page No.
		Daniel Ayre - Deputy Quality Manager	04/12/2018 11:21	1





10501
BH102
8.00 - 8.30







Point Load Results Summary Sheet

Unit 3 Brooklands,
Howden Road,
Tiverton,
Devon
EX16 5HW

Project No.							Project Name												
10501							Watchet Harbour												
Client Job No.							Client												
10501							Internal												
Hole No.	Sample				Specimen Depth	Axial / Diametral / Irregular	THICKNESS (mm) - D	WIDTH (mm) - W	DIAMETER (mm) - D	BREAKING LOAD (kN) - P	D ² _e (mm ²)	Is (MPa)	De	De/50	k _{PLT}	Is 50 (MPa)	Sample Description		
	Ref.	Top	Base	Type															
BH101	-	10.6	10.7	C		A	76.80	79.12		1.2	7736.73	0.16	87.96	1.76	1.29	0.20	Brown MUDSTONE		
BH101	-	11.5	11.6	C		D			79.84	0.3	6373.89	0.05	79.84	1.60	1.23	0.06	Brown MUDSTONE		
BH102	-	8.6	8.7	C		D			78.94	4.4	6231.00	0.71	78.94	1.58	1.23	0.87	Brown MUDSTONE		
BH103	-	9.3	9.4	C		A	78.01	109.52		0	10877.79	0.00	104.30	2.09	1.39	0.00	Brown MUDSTONE (X)		
BH104	-	9.4	9.55	C		A	88.15	79.69		3.2	8944.09	0.36	94.57	1.89	1.33	0.48	Dark grey MUDSTONE		
BH104	-	10.1	10.2	C		D			79.93	0	6388.27	0.00	79.93	1.60	1.24	0.00	Dark grey MUDSTONE (X)		
BH104	-	11.8	11.9	C		D			79.66	0	6346.25	0.00	79.66	1.59	1.23	0.00	Dark grey MUDSTONE (X)		
BH105	-	6.05	6.15	C		D			79.16	5.2	6266.83	0.83	79.16	1.58	1.23	1.02	Grey MUDSTONE		
BH105	-	6.4	6.5	C		I	170.60	74.76		4.7	16238.24	0.29	127.43	2.55	1.52	0.44	Grey MUDSTONE		
BH105	-	9.6	9.7	C		I	30.75	77.35		0	3028.74	0.00	55.03	1.10	1.04	0.00	Grey MUDSTONE (X)		
Wylie and Mah (1991) Rock Slope Engineering						Where a description is followed by (X) this denotes a failure along an existing weakness				Samples tested in accordance with International Journal of Rock Mechanics and Mining. Lab Sheet Reference: KL011R Point Load				Date		Approved By		Page No.	
$I_s = P/D_e^2$ $D_e^2 = (4(WD))/p$ $D_e = \sqrt{D_e^2}$ $I_s(50) = I_s k_{PLT}$ $k_{PLT} = (D_e/50)^{0.45}$														10/12/18		Nick W-W - QM		1	

Appendix G

Geo-environmental Laboratory Test Result



Neil Forrow
South West Geotechnical Ltd
Unit 3 Brooklands
Howden Road
Tiverton
Devon
EX16 5HW

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Unit 1
Rose Lane Industrial Estate
Rose Lane
Lenham Heath
Kent
ME17 2JN
t: 01622 850410
russell.jarvis@dets.co.uk

DETS Report No: 18-85076

Site Reference: Watchet Harbour

Project / Job Ref: 10501/T4026A

Order No: None Supplied

Sample Receipt Date: 13/11/2018

Sample Scheduled Date: 13/11/2018

Report Issue Number: 2

Reporting Date: 07/12/2018

Authorised by:

Russell Jarvis
Associate Director of Client Services

This report supersedes 18-85076.
Opinions and interpretations are outside the laboratory's scope of ISO 17025 accreditation. This certificate is issued in accordance with the accreditation requirements of the United Kingdom Accreditation Service. The results reported herein relate only to the material supplied to the laboratory. This certificate shall not be reproduced except in full, without the prior written approval of the laboratory.



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Lenham Heath
Maidstone
Kent ME17 2JN
Tel : 01622 850410



Soil Analysis Certificate						
DETS Report No: 18-85076	Date Sampled	06/11/18	07/11/18			
South West Geotechnical Ltd	Time Sampled	None Supplied	None Supplied			
Site Reference: Watchet Harbour	TP / BH No	BH101	BH102			
Project / Job Ref: 10501/T4026A	Additional Refs	None Supplied	None Supplied			
Order No: None Supplied	Depth (m)	0.40	0.80			
Reporting Date: 07/12/2018	DETS Sample No	371998	371999			

Determinand	Unit	RL	Accreditation					
Asbestos Screen ^(S)	N/a	N/a	ISO17025	Not Detected	Not Detected			
pH	pH Units	N/a	MCERTS	8.4	7.8			
Total Cyanide	mg/kg	< 2	NONE	< 2	< 2			
W/S Sulphate as SO ₄ (2:1)	mg/l	< 10	MCERTS	56	1420			
W/S Sulphate as SO ₄ (2:1)	g/l	< 0.01	MCERTS	0.06	1.42			
Organic Matter	%	< 0.1	MCERTS	1.8	7.2			
Arsenic (As)	mg/kg	< 2	MCERTS	8	16			
Cadmium (Cd)	mg/kg	< 0.2	MCERTS	0.3	0.3			
Chromium (Cr)	mg/kg	< 2	MCERTS	14	15			
Chromium (hexavalent)	mg/kg	< 2	NONE	< 2	< 2			
Copper (Cu)	mg/kg	< 4	MCERTS	28	138			
Lead (Pb)	mg/kg	< 3	MCERTS	43	284			
Mercury (Hg)	mg/kg	< 1	NONE	< 1	1.8			
Nickel (Ni)	mg/kg	< 3	MCERTS	16	31			
Selenium (Se)	mg/kg	< 3	NONE	< 3	< 3			
Zinc (Zn)	mg/kg	< 3	MCERTS	61	166			

Analytical results are expressed on a dry weight basis where samples are assisted-dried at less than 30°C
Subcontracted analysis (S)



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Maidstone
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Soil Analysis Certificate - Speciated PAHs						
DETS Report No: 18-85076	Date Sampled	06/11/18	07/11/18			
South West Geotechnical Ltd	Time Sampled	None Supplied	None Supplied			
Site Reference: Watchet Harbour	TP / BH No	BH101	BH102			
Project / Job Ref: 10501/T4026A	Additional Refs	None Supplied	None Supplied			
Order No: None Supplied	Depth (m)	0.40	0.80			
Reporting Date: 07/12/2018	DETS Sample No	371998	371999			

Determinand	Unit	RL	Accreditation				
Naphthalene	mg/kg	< 0.1	MCERTS	0.14	0.17		
Acenaphthylene	mg/kg	< 0.1	MCERTS	0.12	< 0.1		
Acenaphthene	mg/kg	< 0.1	MCERTS	0.23	< 0.1		
Fluorene	mg/kg	< 0.1	MCERTS	0.23	< 0.1		
Phenanthrene	mg/kg	< 0.1	MCERTS	1.19	0.32		
Anthracene	mg/kg	< 0.1	MCERTS	0.34	< 0.1		
Fluoranthene	mg/kg	< 0.1	MCERTS	1.52	0.26		
Pyrene	mg/kg	< 0.1	MCERTS	1.50	0.25		
Benzo(a)anthracene	mg/kg	< 0.1	MCERTS	1.02	0.42		
Chrysene	mg/kg	< 0.1	MCERTS	0.70	0.13		
Benzo(b)fluoranthene	mg/kg	< 0.1	MCERTS	1.60	0.47		
Benzo(k)fluoranthene	mg/kg	< 0.1	MCERTS	0.45	< 0.1		
Benzo(a)pyrene	mg/kg	< 0.1	MCERTS	1.11	0.24		
Indeno(1,2,3-cd)pyrene	mg/kg	< 0.1	MCERTS	1.12	0.42		
Dibenz(a,h)anthracene	mg/kg	< 0.1	MCERTS	0.42	< 0.1		
Benzo(ghi)perylene	mg/kg	< 0.1	MCERTS	0.83	0.24		
Total EPA-16 PAHs	mg/kg	< 1.6	MCERTS	12.5	2.9		

Analytical results are expressed on a dry weight basis where samples are assisted-dried at less than 30°C



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Soil Analysis Certificate - TPH CWG Banded						
DETS Report No: 18-85076	Date Sampled	06/11/18	07/11/18			
South West Geotechnical Ltd	Time Sampled	None Supplied	None Supplied			
Site Reference: Watchet Harbour	TP / BH No	BH101	BH102			
Project / Job Ref: 10501/T4026A	Additional Refs	None Supplied	None Supplied			
Order No: None Supplied	Depth (m)	0.40	0.80			
Reporting Date: 07/12/2018	DETS Sample No	371998	371999			

Determinand	Unit	RL	Accreditation					
Aliphatic >C5 - C6	mg/kg	< 0.01	NONE	< 0.01	< 0.01			
Aliphatic >C6 - C8	mg/kg	< 0.05	NONE	< 0.05	< 0.05			
Aliphatic >C8 - C10	mg/kg	< 2	MCERTS	< 2	< 2			
Aliphatic >C10 - C12	mg/kg	< 2	MCERTS	< 2	< 2			
Aliphatic >C12 - C16	mg/kg	< 3	MCERTS	< 3	< 3			
Aliphatic >C16 - C21	mg/kg	< 3	MCERTS	5	< 3			
Aliphatic >C21 - C34	mg/kg	< 10	MCERTS	202	< 10			
Aliphatic (C5 - C34)	mg/kg	< 21	NONE	207	< 21			
Aromatic >C5 - C7	mg/kg	< 0.01	NONE	< 0.01	< 0.01			
Aromatic >C7 - C8	mg/kg	< 0.05	NONE	< 0.05	< 0.05			
Aromatic >C8 - C10	mg/kg	< 2	MCERTS	< 2	< 2			
Aromatic >C10 - C12	mg/kg	< 2	MCERTS	< 2	< 2			
Aromatic >C12 - C16	mg/kg	< 2	MCERTS	< 2	< 2			
Aromatic >C16 - C21	mg/kg	< 3	MCERTS	13	< 3			
Aromatic >C21 - C35	mg/kg	< 10	MCERTS	462	< 10			
Aromatic (C5 - C35)	mg/kg	< 21	NONE	474	< 21			
Total >C5 - C35	mg/kg	< 42	NONE	681	< 42			

Analytical results are expressed on a dry weight basis where samples are assisted-dried at less than 30°C



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Soil Analysis Certificate - BTEX / MTBE						
DETS Report No: 18-85076	Date Sampled	06/11/18	07/11/18			
South West Geotechnical Ltd	Time Sampled	None Supplied	None Supplied			
Site Reference: Watchet Harbour	TP / BH No	BH101	BH102			
Project / Job Ref: 10501/T4026A	Additional Refs	None Supplied	None Supplied			
Order No: None Supplied	Depth (m)	0.40	0.80			
Reporting Date: 07/12/2018	DETS Sample No	371998	371999			

Determinand	Unit	RL	Accreditation					
Benzene	ug/kg	< 2	MCERTS	< 2	< 2			
Toluene	ug/kg	< 5	MCERTS	< 5	< 5			
Ethylbenzene	ug/kg	< 2	MCERTS	< 2	< 2			
p & m-xylene	ug/kg	< 2	MCERTS	6	< 2			
o-xylene	ug/kg	< 2	MCERTS	< 2	< 2			
MTBE	ug/kg	< 5	MCERTS	< 5	< 5			

Analytical results are expressed on a dry weight basis where samples are assisted-dried at less than 30°C



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Waste Acceptance Criteria Analytical Certificate - BS EN 12457/3										
DETS Report No: 18-85076		Date Sampled		07/11/18		Landfill Waste Acceptance Criteria Limits				
South West Geotechnical Ltd		Time Sampled		None Supplied						
Site Reference: Watchet Harbour		TP / BH No		BH102						
Project / Job Ref: 10501/T4026A		Additional Refs		None Supplied						
Order No: None Supplied		Depth (m)		0.80						
Reporting Date: 07/12/2018		DETS Sample No		371999						
Determinand	Unit	MDL								
TOC ^{MU}	%	< 0.1	4.2							
Loss on Ignition	%	< 0.01	16.50							
BTEX ^{MU}	mg/kg	< 0.05	< 0.05							
Sum of PCBs	mg/kg	< 0.1	< 0.1							
Mineral Oil ^{MU}	mg/kg	< 10	< 10							
Total PAH ^{MU}	mg/kg	< 1.7	2.9							
pH ^{MU}	pH Units	N/a	7.8							
Acid Neutralisation Capacity	mol/kg (+/-)	< 1	1.9							
Eluate Analysis				2:1 mg/l	8:1 mg/l		Cumulative 10:1 mg/kg	Limit values for compliance leaching test using BS EN 12457-3 at L/S 10 l/kg (mg/kg)		
Arsenic ^U				< 0.01	< 0.01		< 0.2	0.5	2	25
Barium ^U				0.05	0.05		0.5	20	100	300
Cadmium ^U				< 0.0005	< 0.0005		< 0.02	0.04	1	5
Chromium ^U				< 0.005	< 0.005		< 0.20	0.5	10	70
Copper ^U				< 0.01	< 0.01		< 0.5	2	50	100
Mercury ^U				< 0.005	< 0.005		< 0.01	0.01	0.2	2
Molybdenum ^U				0.028	0.010		0.1	0.5	10	30
Nickel ^U				< 0.007	< 0.007		< 0.2	0.4	10	40
Lead ^U				< 0.005	< 0.005		< 0.2	0.5	10	50
Antimony ^U				0.017	0.012		0.12	0.06	0.7	5
Selenium ^U				< 0.005	< 0.005		< 0.1	0.1	0.5	7
Zinc ^U				0.006	< 0.005		< 0.2	4	50	200
Chloride ^U				9	1		24	800	15000	25000
Fluoride ^U				< 0.5	< 0.5		< 1	10	150	500
Sulphate ^U				524	45		1079	1000	20000	50000
TDS				555	114		1722	4000	60000	100000
Phenol Index				< 0.01	< 0.01		< 0.5	1	-	-
DOC				4.6	7.1		67.9	500	800	1000
Leach Test Information										
Sample Mass (kg)				0.20						
Dry Matter (%)				87.8						
Moisture (%)				14						
Stage 1										
Volume Eluate L2 (litres)				0.33						
Filtered Eluate VE1 (litres)				0.23						
Results are expressed on a dry weight basis, after correction for moisture content where applicable Stated limits are for guidance only and QTS Environmental cannot be held responsible for any discrepancies with current legislation M Denotes MCERTS accredited test U Denotes ISO17025 accredited test										



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Lenham Heath
Maidstone
Kent ME17 2JN
Tel : 01622 850410



Soil Analysis Certificate - Sample Descriptions	
DETS Report No: 18-85076	
South West Geotechnical Ltd	
Site Reference: Watchet Harbour	
Project / Job Ref: 10501/T4026A	
Order No: None Supplied	
Reporting Date: 07/12/2018	

DETS Sample No	TP / BH No	Additional Refs	Depth (m)	Moisture Content (%)	Sample Matrix Description
371998	BH101	None Supplied	0.40	4.5	Brown sandy gravel with stones and concrete
371999	BH102	None Supplied	0.80	12.2	Black sandy clay with stones

Moisture content is part of procedure E003 & is not an accredited test
Insufficient Sample ^{I/S}
Unsuitable Sample ^{U/S}



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Rose Lane
Lenham Heath
Maidstone
Kent ME17 2JN
Tel : 01622 850410



Soil Analysis Certificate - Methodology & Miscellaneous Information				
DETS Report No: 18-85076				
South West Geotechnical Ltd				
Site Reference: Watchet Harbour				
Project / Job Ref: 10501/T4026A				
Order No: None Supplied				
Reporting Date: 07/12/2018				

Matrix	Analysed On	Determinand	Brief Method Description	Method No
Soil	D	Boron - Water Soluble	Determination of water soluble boron in soil by 2:1 hot water extract followed by ICP-OES	E012
Soil	AR	BTEX	Determination of BTEX by headspace GC-MS	E001
Soil	D	Cations	Determination of cations in soil by aqua-regia digestion followed by ICP-OES	E002
Soil	D	Chloride - Water Soluble (2:1)	Determination of chloride by extraction with water & analysed by ion chromatography	E009
Soil	AR	Chromium - Hexavalent	Determination of hexavalent chromium in soil by extraction in water then by acidification, addition of 1,5 diphenylcarbazide followed by colorimetry	E016
Soil	AR	Cyanide - Complex	Determination of complex cyanide by distillation followed by colorimetry	E015
Soil	AR	Cyanide - Free	Determination of free cyanide by distillation followed by colorimetry	E015
Soil	AR	Cyanide - Total	Determination of total cyanide by distillation followed by colorimetry	E015
Soil	D	Cyclohexane Extractable Matter (CEM)	Gravimetrically determined through extraction with cyclohexane	E011
Soil	AR	Diesel Range Organics (C10 - C24)	Determination of hexane/acetone extractable hydrocarbons by GC-FID	E004
Soil	AR	Electrical Conductivity	Determination of electrical conductivity by addition of saturated calcium sulphate followed by electrometric measurement	E022
Soil	AR	Electrical Conductivity	Determination of electrical conductivity by addition of water followed by electrometric measurement	E023
Soil	D	Elemental Sulphur	Determination of elemental sulphur by solvent extraction followed by GC-MS	E020
Soil	AR	EPH (C10 – C40)	Determination of acetone/hexane extractable hydrocarbons by GC-FID	E004
Soil	AR	EPH Product ID	Determination of acetone/hexane extractable hydrocarbons by GC-FID	E004
Soil	AR	EPH TEXAS (C6-C8, C8-C10, C10-C12, C12-C16, C16-C21, C21-C40)	Determination of acetone/hexane extractable hydrocarbons by GC-FID for C8 to C40. C6 to C8 by headspace GC-MS	E004
Soil	D	Fluoride - Water Soluble	Determination of Fluoride by extraction with water & analysed by ion chromatography	E009
Soil	D	FOC (Fraction Organic Carbon)	Determination of fraction of organic carbon by oxidising with potassium dichromate followed by titration with iron (II) sulphate	E010
Soil	D	Loss on Ignition @ 450oC	Determination of loss on ignition in soil by gravimetrically with the sample being ignited in a muffle furnace	E019
Soil	D	Magnesium - Water Soluble	Determination of water soluble magnesium by extraction with water followed by ICP-OES	E025
Soil	D	Metals	Determination of metals by aqua-regia digestion followed by ICP-OES	E002
Soil	AR	Mineral Oil (C10 - C40)	Determination of hexane/acetone extractable hydrocarbons by GC-FID fractionating with SPE cartridge	E004
Soil	AR	Moisture Content	Moisture content: determined gravimetrically	E003
Soil	D	Nitrate - Water Soluble (2:1)	Determination of nitrate by extraction with water & analysed by ion chromatography	E009
Soil	D	Organic Matter	Determination of organic matter by oxidising with potassium dichromate followed by titration with iron (II) sulphate	E010
Soil	AR	PAH - Speciated (EPA 16)	Determination of PAH compounds by extraction in acetone and hexane followed by GC-MS with the use of surrogate and internal standards	E005
Soil	AR	PCB - 7 Congeners	Determination of PCB by extraction with acetone and hexane followed by GC-MS	E008
Soil	D	Petroleum Ether Extract (PEE)	Gravimetrically determined through extraction with petroleum ether	E011
Soil	AR	pH	Determination of pH by addition of water followed by electrometric measurement	E007
Soil	AR	Phenols - Total (monohydric)	Determination of phenols by distillation followed by colorimetry	E021
Soil	D	Phosphate - Water Soluble (2:1)	Determination of phosphate by extraction with water & analysed by ion chromatography	E009
Soil	D	Sulphate (as SO4) - Total	Determination of total sulphate by extraction with 10% HCl followed by ICP-OES	E013
Soil	D	Sulphate (as SO4) - Water Soluble (2:1)	Determination of sulphate by extraction with water & analysed by ion chromatography	E009
Soil	D	Sulphate (as SO4) - Water Soluble (2:1)	Determination of water soluble sulphate by extraction with water followed by ICP-OES	E014
Soil	AR	Sulphide	Determination of sulphide by distillation followed by colorimetry	E018
Soil	D	Sulphur - Total	Determination of total sulphur by extraction with aqua-regia followed by ICP-OES	E024
Soil	AR	SVOC	Determination of semi-volatile organic compounds by extraction in acetone and hexane followed by GC-MS	E006
Soil	AR	Thiocyanate (as SCN)	Determination of thiocyanate by extraction in caustic soda followed by acidification followed by addition of ferric nitrate followed by colorimetry	E017
Soil	D	Toluene Extractable Matter (TEM)	Gravimetrically determined through extraction with toluene	E011
Soil	D	Total Organic Carbon (TOC)	Determination of organic matter by oxidising with potassium dichromate followed by titration with iron (II) sulphate	E010
Soil	AR	TPH CWG (ali: C5- C6, C6-C8, C8-C10, C10-C12, C12-C16, C16-C21, C21-C34, aro: C5-C7, C7-C8, C8-C10, C10-C12, C12-C16, C16-C21, C21-C35)	Determination of hexane/acetone extractable hydrocarbons by GC-FID fractionating with SPE cartridge for C8 to C35. C5 to C8 by headspace GC-MS	E004
Soil	AR	TPH LQM (ali: C5-C6, C6-C8, C8-C10, C10-C12, C12-C16, C16-C35, C35-C44, aro: C5-C7, C7-C8, C8-C10, C10-C12, C12-C16, C16-C21, C21-C35, C35-C44)	Determination of hexane/acetone extractable hydrocarbons by GC-FID fractionating with SPE cartridge for C8 to C44. C5 to C8 by headspace GC-MS	E004
Soil	AR	VOCs	Determination of volatile organic compounds by headspace GC-MS	E001
Soil	AR	VPH (C6-C8 & C8-C10)	Determination of hydrocarbons C6-C8 by headspace GC-MS & C8-C10 by GC-FID	E001

D Dried
AR As Received



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DETS Report No: 18-85540

Site Reference: Watchet Harbour

Project / Job Ref: 10501 / T4026B

Order No: None Supplied

Sample Receipt Date: 22/11/2018

Sample Scheduled Date: 22/11/2018

Report Issue Number: 1

Reporting Date: 28/11/2018

Authorised by:

A handwritten signature in black ink, appearing to read "Dave Ashworth".

Dave Ashworth
Deputy Quality Manager

Authorised by:



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Soil Analysis Certificate						
DETS Report No: 18-85540	Date Sampled	08/11/18	08/11/18	09/11/18	09/11/18	13/11/18
South West Geotechnical Ltd	Time Sampled	None Supplied	None Supplied	None Supplied	None Supplied	None Supplied
Site Reference: Watchet Harbour	TP / BH No	BH102	BH102	BH103	BH103	BH104
Project / Job Ref: 10501 / T4026B	Additional Refs	None Supplied	None Supplied	None Supplied	None Supplied	None Supplied
Order No: None Supplied	Depth (m)	1.40 - 2.70	4.60	0.50	3.20	3.20 - 4.20
Reporting Date: 28/11/2018	DETS Sample No	374058	374059	374061	374062	374063

Determinand	Unit	RL	Accreditation					
Asbestos Screen ^(S)	N/a	N/a	ISO17025			Not Detected		
pH	pH Units	N/a	MCERTS	7.8	8.0	10.0	8.6	8.8
Total Cyanide	mg/kg	< 2	NONE			< 2		
W/S Sulphate as SO ₄ (2:1)	mg/l	< 10	MCERTS	775	609	47	295	251
W/S Sulphate as SO ₄ (2:1)	g/l	< 0.01	MCERTS	0.77	0.61	0.05	0.30	0.25
Organic Matter	%	< 0.1	MCERTS			0.5		
Arsenic (As)	mg/kg	< 2	MCERTS			17		
Cadmium (Cd)	mg/kg	< 0.2	MCERTS			< 0.2		
Chromium (Cr)	mg/kg	< 2	MCERTS			18		
Chromium (hexavalent)	mg/kg	< 2	NONE			< 2		
Copper (Cu)	mg/kg	< 4	MCERTS			23		
Lead (Pb)	mg/kg	< 3	MCERTS			10		
Mercury (Hg)	mg/kg	< 1	NONE			< 1		
Nickel (Ni)	mg/kg	< 3	MCERTS			26		
Selenium (Se)	mg/kg	< 3	NONE			< 3		
Zinc (Zn)	mg/kg	< 3	MCERTS			36		

Analytical results are expressed on a dry weight basis where samples are assisted-dried at less than 30^oC
Subcontracted analysis (S)



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Soil Analysis Certificate						
DETS Report No: 18-85540	Date Sampled	13/11/18	14/11/18			
South West Geotechnical Ltd	Time Sampled	None Supplied	None Supplied			
Site Reference: Watchet Harbour	TP / BH No	BH104	BH105			
Project / Job Ref: 10501 / T4026B	Additional Refs	None Supplied	None Supplied			
Order No: None Supplied	Depth (m)	4.50	1.00			
Reporting Date: 28/11/2018	DETS Sample No	374064	374065			

Determinand	Unit	RL	Accreditation					
Asbestos Screen ^(S)	N/a	N/a	ISO17025	Not Detected	Not Detected			
pH	pH Units	N/a	MCERTS	9.0	5.7			
Total Cyanide	mg/kg	< 2	NONE	< 2	< 2			
W/S Sulphate as SO ₄ (2:1)	mg/l	< 10	MCERTS	240	27			
W/S Sulphate as SO ₄ (2:1)	g/l	< 0.01	MCERTS	0.24	0.03			
Organic Matter	%	< 0.1	MCERTS	1.5	1.2			
Arsenic (As)	mg/kg	< 2	MCERTS	7	13			
Cadmium (Cd)	mg/kg	< 0.2	MCERTS	1.4	0.3			
Chromium (Cr)	mg/kg	< 2	MCERTS	10	14			
Chromium (hexavalent)	mg/kg	< 2	NONE	< 2	< 2			
Copper (Cu)	mg/kg	< 4	MCERTS	22	23			
Lead (Pb)	mg/kg	< 3	MCERTS	16	36			
Mercury (Hg)	mg/kg	< 1	NONE	< 1	< 1			
Nickel (Ni)	mg/kg	< 3	MCERTS	15	22			
Selenium (Se)	mg/kg	< 3	NONE	< 3	< 3			
Zinc (Zn)	mg/kg	< 3	MCERTS	222	96			

Analytical results are expressed on a dry weight basis where samples are assisted-dried at less than 30°C
Subcontracted analysis (S)



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Soil Analysis Certificate - Speciated PAHs						
DETS Report No: 18-85540	Date Sampled	09/11/18	13/11/18	14/11/18		
South West Geotechnical Ltd	Time Sampled	None Supplied	None Supplied	None Supplied		
Site Reference: Watchet Harbour	TP / BH No	BH103	BH104	BH105		
Project / Job Ref: 10501 / T4026B	Additional Refs	None Supplied	None Supplied	None Supplied		
Order No: None Supplied	Depth (m)	0.50	4.50	1.00		
Reporting Date: 28/11/2018	DETS Sample No	374061	374064	374065		

Determinand	Unit	RL	Accreditation					
Naphthalene	mg/kg	< 0.1	MCERTS	< 0.1	< 0.1	< 0.1		
Acenaphthylene	mg/kg	< 0.1	MCERTS	< 0.1	< 0.1	< 0.1		
Acenaphthene	mg/kg	< 0.1	MCERTS	< 0.1	< 0.1	< 0.1		
Fluorene	mg/kg	< 0.1	MCERTS	< 0.1	< 0.1	< 0.1		
Phenanthrene	mg/kg	< 0.1	MCERTS	< 0.1	< 0.1	< 0.1		
Anthracene	mg/kg	< 0.1	MCERTS	< 0.1	< 0.1	< 0.1		
Fluoranthene	mg/kg	< 0.1	MCERTS	0.11	< 0.1	< 0.1		
Pyrene	mg/kg	< 0.1	MCERTS	< 0.1	< 0.1	< 0.1		
Benzo(a)anthracene	mg/kg	< 0.1	MCERTS	< 0.1	< 0.1	< 0.1		
Chrysene	mg/kg	< 0.1	MCERTS	< 0.1	< 0.1	< 0.1		
Benzo(b)fluoranthene	mg/kg	< 0.1	MCERTS	0.12	< 0.1	< 0.1		
Benzo(k)fluoranthene	mg/kg	< 0.1	MCERTS	< 0.1	< 0.1	< 0.1		
Benzo(a)pyrene	mg/kg	< 0.1	MCERTS	< 0.1	< 0.1	< 0.1		
Indeno(1,2,3-cd)pyrene	mg/kg	< 0.1	MCERTS	0.17	< 0.1	< 0.1		
Dibenz(a,h)anthracene	mg/kg	< 0.1	MCERTS	< 0.1	< 0.1	< 0.1		
Benzo(ghi)perylene	mg/kg	< 0.1	MCERTS	0.20	< 0.1	< 0.1		
Total EPA-16 PAHs	mg/kg	< 1.6	MCERTS	< 1.6	< 1.6	< 1.6		

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Soil Analysis Certificate - TPH CWG Banded						
DETS Report No: 18-85540	Date Sampled	09/11/18	13/11/18	14/11/18		
South West Geotechnical Ltd	Time Sampled	None Supplied	None Supplied	None Supplied		
Site Reference: Watchet Harbour	TP / BH No	BH103	BH104	BH105		
Project / Job Ref: 10501 / T4026B	Additional Refs	None Supplied	None Supplied	None Supplied		
Order No: None Supplied	Depth (m)	0.50	4.50	1.00		
Reporting Date: 28/11/2018	DETS Sample No	374061	374064	374065		

Determinand	Unit	RL	Accreditation					
Aliphatic >C5 - C6	mg/kg	< 0.01	NONE	< 0.01	< 0.01	< 0.01		
Aliphatic >C6 - C8	mg/kg	< 0.05	NONE	< 0.05	< 0.05	< 0.05		
Aliphatic >C8 - C10	mg/kg	< 2	MCERTS	< 2	< 2	< 2		
Aliphatic >C10 - C12	mg/kg	< 2	MCERTS	< 2	< 2	< 2		
Aliphatic >C12 - C16	mg/kg	< 3	MCERTS	< 3	< 3	< 3		
Aliphatic >C16 - C21	mg/kg	< 3	MCERTS	< 3	< 3	< 3		
Aliphatic >C21 - C34	mg/kg	< 10	MCERTS	< 10	< 10	< 10		
Aliphatic (C5 - C34)	mg/kg	< 21	NONE	< 21	< 21	< 21		
Aromatic >C5 - C7	mg/kg	< 0.01	NONE	< 0.01	< 0.01	< 0.01		
Aromatic >C7 - C8	mg/kg	< 0.05	NONE	< 0.05	< 0.05	< 0.05		
Aromatic >C8 - C10	mg/kg	< 2	MCERTS	< 2	< 2	< 2		
Aromatic >C10 - C12	mg/kg	< 2	MCERTS	< 2	< 2	< 2		
Aromatic >C12 - C16	mg/kg	< 2	MCERTS	< 2	< 2	< 2		
Aromatic >C16 - C21	mg/kg	< 3	MCERTS	< 3	< 3	< 3		
Aromatic >C21 - C35	mg/kg	< 10	MCERTS	< 10	< 10	< 10		
Aromatic (C5 - C35)	mg/kg	< 21	NONE	< 21	< 21	< 21		
Total >C5 - C35	mg/kg	< 42	NONE	< 42	< 42	< 42		

Analytical results are expressed on a dry weight basis where samples are assisted-dried at less than 30°C



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Soil Analysis Certificate - BTEX / MTBE						
DETS Report No: 18-85540	Date Sampled	09/11/18	13/11/18	14/11/18		
South West Geotechnical Ltd	Time Sampled	None Supplied	None Supplied	None Supplied		
Site Reference: Watchet Harbour	TP / BH No	BH103	BH104	BH105		
Project / Job Ref: 10501 / T4026B	Additional Refs	None Supplied	None Supplied	None Supplied		
Order No: None Supplied	Depth (m)	0.50	4.50	1.00		
Reporting Date: 28/11/2018	DETS Sample No	374061	374064	374065		

Determinand	Unit	RL	Accreditation					
Benzene	ug/kg	< 2	MCERTS	< 2	< 2	< 2		
Toluene	ug/kg	< 5	MCERTS	< 5	< 5	< 5		
Ethylbenzene	ug/kg	< 2	MCERTS	< 2	< 2	< 2		
p & m-xylene	ug/kg	< 2	MCERTS	< 2	< 2	< 2		
o-xylene	ug/kg	< 2	MCERTS	< 2	< 2	< 2		
MTBE	ug/kg	< 5	MCERTS	< 5	< 5	< 5		

Analytical results are expressed on a dry weight basis where samples are assisted-dried at less than 30°C



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Waste Acceptance Criteria Analytical Certificate - BS EN 12457/3									
DETS Report No: 18-85540		Date Sampled	13/11/18			Landfill Waste Acceptance Criteria Limits			
South West Geotechnical Ltd		Time Sampled	None Supplied						
Site Reference: Watchet Harbour		TP / BH No	BH104						
Project / Job Ref: 10501 / T4026B		Additional Refs	None Supplied						
Order No: None Supplied		Depth (m)	4.50						
Reporting Date: 28/11/2018		DETS Sample No	374064						
Determinand	Unit	MDL							
TOC ^{MU}	%	< 0.1	0.9			3%			
Loss on Ignition	%	< 0.01	2.30			--			
BTEX ^{MU}	mg/kg	< 0.05	< 0.05			6			
Sum of PCBs	mg/kg	< 0.1	< 0.1			1			
Mineral Oil ^{MU}	mg/kg	< 10	< 10			500			
Total PAH ^{MU}	mg/kg	< 1.7	< 1.7			100			
pH ^{MU}	pH Units	N/a	9.0			--			
Acid Neutralisation Capacity	mol/kg (+/-)	< 1	2.5			--			
Eluate Analysis			2:1 mg/l	8:1 mg/l		Cumulative 10:1 mg/kg	Limit values for compliance leaching test using BS EN 12457-3 at L/S 10 l/kg (mg/kg)		
Arsenic ^U			< 0.01	< 0.01		< 0.2	0.5	2	25
Barium ^U			0.02	< 0.02		< 0.1	20	100	300
Cadmium ^U			< 0.0005	< 0.0005		< 0.02	0.04	1	5
Chromium ^U			< 0.005	< 0.005		< 0.20	0.5	10	70
Copper ^U			< 0.01	< 0.01		< 0.5	2	50	100
Mercury ^U			< 0.005	< 0.005		< 0.01	0.01	0.2	2
Molybdenum ^U			0.054	0.020		0.2	0.5	10	30
Nickel ^U			< 0.007	< 0.007		< 0.2	0.4	10	40
Lead ^U			< 0.005	< 0.005		< 0.2	0.5	10	50
Antimony ^U			< 0.005	< 0.005		< 0.06	0.06	0.7	5
Selenium ^U			< 0.005	< 0.005		< 0.1	0.1	0.5	7
Zinc ^U			< 0.005	< 0.005		< 0.2	4	50	200
Chloride ^U			675	75		1340	800	15000	25000
Fluoride ^U			1.2	0.6		6.6	10	150	500
Sulphate ^U			147	21		338	1000	20000	50000
TDS			1260	241		3409	4000	60000	100000
Phenol Index			< 0.01	< 0.01		< 0.5	1	-	-
DOC			5.7	10.4		99.2	500	800	1000
Leach Test Information									
Sample Mass (kg)			0.19						
Dry Matter (%)			92.3						
Moisture (%)			8.4						
Stage 1									
Volume Eluate L2 (litres)			0.34						
Filtered Eluate VE1 (litres)			0.17						
Results are expressed on a dry weight basis, after correction for moisture content where applicable Stated limits are for guidance only and QTS Environmental cannot be held responsible for any discrepancies with current legislation M Denotes MCERTS accredited test U Denotes ISO17025 accredited test									



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Soil Analysis Certificate - Sample Descriptions	
DETS Report No: 18-85540	
South West Geotechnical Ltd	
Site Reference: Watchet Harbour	
Project / Job Ref: 10501 / T4026B	
Order No: None Supplied	
Reporting Date: 28/11/2018	

DETS Sample No	TP / BH No	Additional Refs	Depth (m)	Moisture Content (%)	Sample Matrix Description
\$ 374058	BH102	None Supplied	1.40 - 2.70	12.6	Black sandy clay with stones
\$ 374059	BH102	None Supplied	4.60	23.4	Brown clay with stones
\$ 374061	BH103	None Supplied	0.50	7	Red sandy clay with stones
\$ 374062	BH103	None Supplied	3.20	13.6	Red sandy clay with stones
374063	BH104	None Supplied	3.20 - 4.20	11.5	Brown sandy clay with stones
374064	BH104	None Supplied	4.50	7.7	Brown sandy clay with stones
374065	BH105	None Supplied	1.00	11	Brown sandy clay with stones

Moisture content is part of procedure E003 & is not an accredited test

Insufficient Sample ^{I/S}

Unsuitable Sample ^{U/S}

\$ samples exceeded recommended holding times



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Soil Analysis Certificate - Methodology & Miscellaneous Information				
DETS Report No: 18-85540				
South West Geotechnical Ltd				
Site Reference: Watchet Harbour				
Project / Job Ref: 10501 / T4026B				
Order No: None Supplied				
Reporting Date: 28/11/2018				

Matrix	Analysed On	Determinand	Brief Method Description	Method No
Soil	D	Boron - Water Soluble	Determination of water soluble boron in soil by 2:1 hot water extract followed by ICP-OES	E012
Soil	AR	BTEX	Determination of BTEX by headspace GC-MS	E001
Soil	D	Cations	Determination of cations in soil by aqua-regia digestion followed by ICP-OES	E002
Soil	D	Chloride - Water Soluble (2:1)	Determination of chloride by extraction with water & analysed by ion chromatography	E009
Soil	AR	Chromium - Hexavalent	Determination of hexavalent chromium in soil by extraction in water then by acidification, addition of 1,5 diphenylcarbazide followed by colorimetry	E016
Soil	AR	Cyanide - Complex	Determination of complex cyanide by distillation followed by colorimetry	E015
Soil	AR	Cyanide - Free	Determination of free cyanide by distillation followed by colorimetry	E015
Soil	AR	Cyanide - Total	Determination of total cyanide by distillation followed by colorimetry	E015
Soil	D	Cyclohexane Extractable Matter (CEM)	Gravimetrically determined through extraction with cyclohexane	E011
Soil	AR	Diesel Range Organics (C10 - C24)	Determination of hexane/acetone extractable hydrocarbons by GC-FID	E004
Soil	AR	Electrical Conductivity	Determination of electrical conductivity by addition of saturated calcium sulphate followed by electrometric measurement	E022
Soil	AR	Electrical Conductivity	Determination of electrical conductivity by addition of water followed by electrometric measurement	E023
Soil	D	Elemental Sulphur	Determination of elemental sulphur by solvent extraction followed by GC-MS	E020
Soil	AR	EPH (C10 – C40)	Determination of acetone/hexane extractable hydrocarbons by GC-FID	E004
Soil	AR	EPH Product ID	Determination of acetone/hexane extractable hydrocarbons by GC-FID	E004
Soil	AR	EPH TEXAS (C6-C8, C8-C10, C10-C12, C12-C16, C16-C21, C21-C40)	Determination of acetone/hexane extractable hydrocarbons by GC-FID for C8 to C40. C6 to C8 by headspace GC-MS	E004
Soil	D	Fluoride - Water Soluble	Determination of Fluoride by extraction with water & analysed by ion chromatography	E009
Soil	D	FOC (Fraction Organic Carbon)	Determination of fraction of organic carbon by oxidising with potassium dichromate followed by titration with iron (II) sulphate	E010
Soil	D	Loss on Ignition @ 450oC	Determination of loss on ignition in soil by gravimetrically with the sample being ignited in a muffle furnace	E019
Soil	D	Magnesium - Water Soluble	Determination of water soluble magnesium by extraction with water followed by ICP-OES	E025
Soil	D	Metals	Determination of metals by aqua-regia digestion followed by ICP-OES	E002
Soil	AR	Mineral Oil (C10 - C40)	Determination of hexane/acetone extractable hydrocarbons by GC-FID fractionating with SPE cartridge	E004
Soil	AR	Moisture Content	Moisture content: determined gravimetrically	E003
Soil	D	Nitrate - Water Soluble (2:1)	Determination of nitrate by extraction with water & analysed by ion chromatography	E009
Soil	D	Organic Matter	Determination of organic matter by oxidising with potassium dichromate followed by titration with iron (II) sulphate	E010
Soil	AR	PAH - Speciated (EPA 16)	Determination of PAH compounds by extraction in acetone and hexane followed by GC-MS with the use of surrogate and internal standards	E005
Soil	AR	PCB - 7 Congeners	Determination of PCB by extraction with acetone and hexane followed by GC-MS	E008
Soil	D	Petroleum Ether Extract (PEE)	Gravimetrically determined through extraction with petroleum ether	E011
Soil	AR	pH	Determination of pH by addition of water followed by electrometric measurement	E007
Soil	AR	Phenols - Total (monohydric)	Determination of phenols by distillation followed by colorimetry	E021
Soil	D	Phosphate - Water Soluble (2:1)	Determination of phosphate by extraction with water & analysed by ion chromatography	E009
Soil	D	Sulphate (as SO4) - Total	Determination of total sulphate by extraction with 10% HCl followed by ICP-OES	E013
Soil	D	Sulphate (as SO4) - Water Soluble (2:1)	Determination of sulphate by extraction with water & analysed by ion chromatography	E009
Soil	D	Sulphate (as SO4) - Water Soluble (2:1)	Determination of water soluble sulphate by extraction with water followed by ICP-OES	E014
Soil	AR	Sulphide	Determination of sulphide by distillation followed by colorimetry	E018
Soil	D	Sulphur - Total	Determination of total sulphur by extraction with aqua-regia followed by ICP-OES	E024
Soil	AR	SVOC	Determination of semi-volatile organic compounds by extraction in acetone and hexane followed by GC-MS	E006
Soil	AR	Thiocyanate (as SCN)	Determination of thiocyanate by extraction in caustic soda followed by acidification followed by addition of ferric nitrate followed by colorimetry	E017
Soil	D	Toluene Extractable Matter (TEM)	Gravimetrically determined through extraction with toluene	E011
Soil	D	Total Organic Carbon (TOC)	Determination of organic matter by oxidising with potassium dichromate followed by titration with iron (II) sulphate	E010
Soil	AR	TPH CWG (ali: C5- C6, C6-C8, C8-C10, C10-C12, C12-C16, C16-C21, C21-C34, aro: C5-C7, C7-C8, C8-C10, C10-C12, C12-C16, C16-C21, C21-C35)	Determination of hexane/acetone extractable hydrocarbons by GC-FID fractionating with SPE cartridge for C8 to C35. C5 to C8 by headspace GC-MS	E004
Soil	AR	TPH LQM (ali: C5-C6, C6-C8, C8-C10, C10-C12, C12-C16, C16-C35, C35-C44, aro: C5-C7, C7-C8, C8-C10, C10-C12, C12-C16, C16-C21, C21-C35, C35-C44)	Determination of hexane/acetone extractable hydrocarbons by GC-FID fractionating with SPE cartridge for C8 to C44. C5 to C8 by headspace GC-MS	E004
Soil	AR	VOCs	Determination of volatile organic compounds by headspace GC-MS	E001
Soil	AR	VPH (C6-C8 & C8-C10)	Determination of hydrocarbons C6-C8 by headspace GC-MS & C8-C10 by GC-FID	E001

D Dried
AR As Received



Neil Forrow
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t: 01622 850410
russell.jarvis@dets.co.uk

DETS Report No: 18-86156

Site Reference: Watchet Harbour

Project / Job Ref: 10501 / T4026B

Order No: None Supplied

Sample Receipt Date: 04/12/2018

Sample Scheduled Date: 04/12/2018

Report Issue Number: 1

Reporting Date: 10/12/2018

Authorised by:

A handwritten signature in black ink, appearing to read "R Jarvis", written over a horizontal line.

Russell Jarvis
Associate Director of Client Services

Opinions and interpretations are outside the laboratory's scope of ISO 17025 accreditation. This certificate is issued in accordance with the accreditation requirements of the United Kingdom Accreditation Service. The results reported herein relate only to the material supplied to the laboratory. This certificate shall not be reproduced except in full, without the prior written approval of the laboratory.



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Soil Analysis Certificate						
DETS Report No: 18-86156	Date Sampled	08/11/18	15/11/18			
South West Geotechnical Ltd	Time Sampled	None Supplied	None Supplied			
Site Reference: Watchet Harbour	TP / BH No	BH102	BH105			
Project / Job Ref: 10501 / T4026B	Additional Refs	None Supplied	None Supplied			
Order No: None Supplied	Depth (m)	9.30 - 9.40	6.60			
Reporting Date: 10/12/2018	DETS Sample No	376588	376589			

Determinand	Unit	RL	Accreditation					
pH	pH Units	N/a	MCERTS	8.7	8.0			
W/S Sulphate as SO ₄ (2:1)	mg/l	< 10	MCERTS	62	480			
W/S Sulphate as SO ₄ (2:1)	g/l	< 0.01	MCERTS	0.06	0.48			

Analytical results are expressed on a dry weight basis where samples are assisted-dried at less than 30^oC
Subcontracted analysis (S)



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Soil Analysis Certificate - Sample Descriptions	
DETS Report No: 18-86156	
South West Geotechnical Ltd	
Site Reference: Watchet Harbour	
Project / Job Ref: 10501 / T4026B	
Order No: None Supplied	
Reporting Date: 10/12/2018	

DETS Sample No	TP / BH No	Additional Refs	Depth (m)	Moisture Content (%)	Sample Matrix Description
\$ 376588	BH102	None Supplied	9.30 - 9.40	4.6	Red sandy clay
\$ 376589	BH105	None Supplied	6.60	4.5	Black sandy clay with stones

Moisture content is part of procedure E003 & is not an accredited test
Insufficient Sample ^{I/S}
Unsuitable Sample ^{U/S}

\$ samples exceeded recommended holding times



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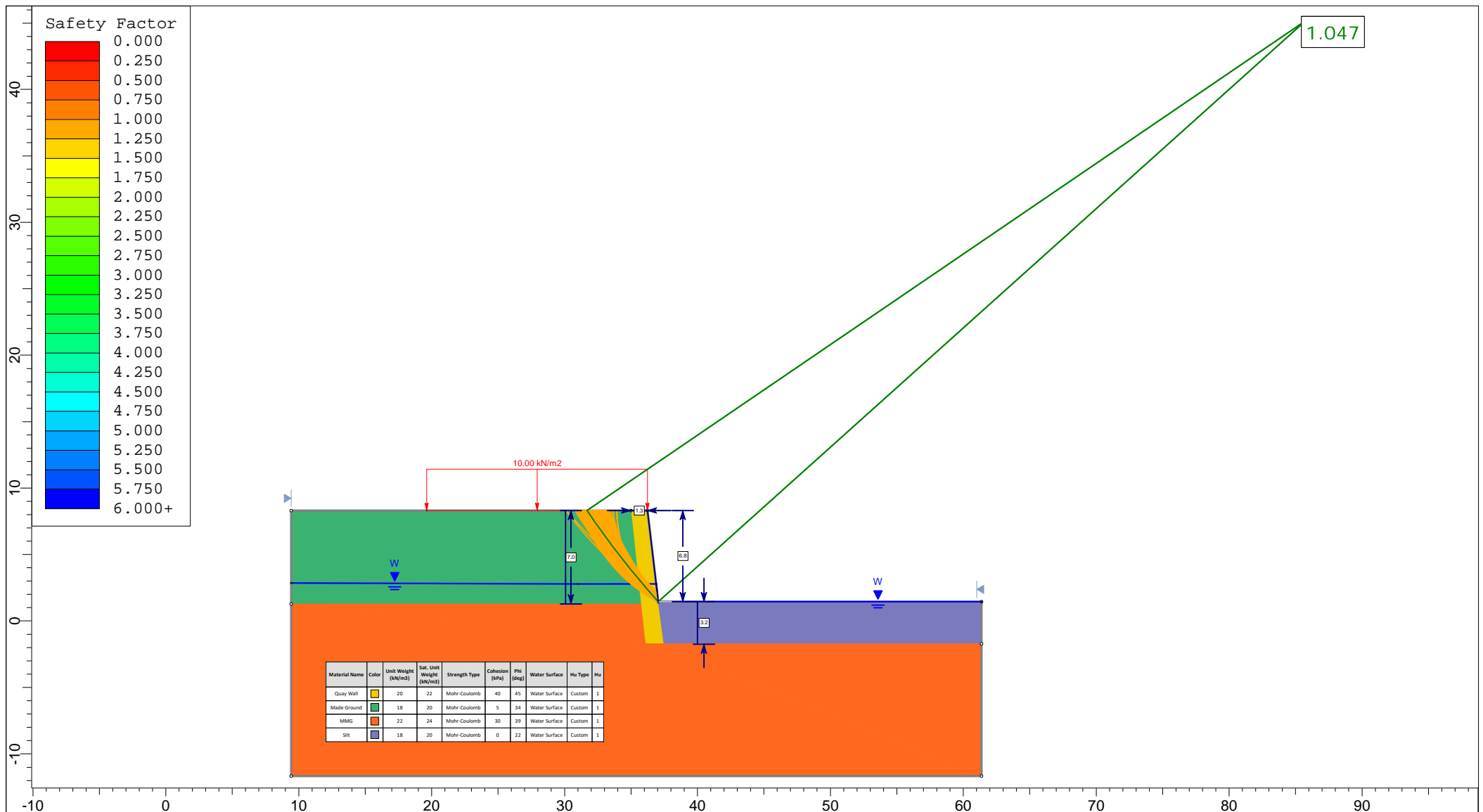
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DETS Report No: 18-86156				
South West Geotechnical Ltd				
Site Reference: Watchet Harbour				
Project / Job Ref: 10501 / T4026B				
Order No: None Supplied				
Reporting Date: 10/12/2018				

Matrix	Analysed On	Determinand	Brief Method Description	Method No
Soil	D	Boron - Water Soluble	Determination of water soluble boron in soil by 2:1 hot water extract followed by ICP-OES	E012
Soil	AR	BTEX	Determination of BTEX by headspace GC-MS	E001
Soil	D	Cations	Determination of cations in soil by aqua-regia digestion followed by ICP-OES	E002
Soil	D	Chloride - Water Soluble (2:1)	Determination of chloride by extraction with water & analysed by ion chromatography	E009
Soil	AR	Chromium - Hexavalent	Determination of hexavalent chromium in soil by extraction in water then by acidification, addition of 1,5 diphenylcarbazide followed by colorimetry	E016
Soil	AR	Cyanide - Complex	Determination of complex cyanide by distillation followed by colorimetry	E015
Soil	AR	Cyanide - Free	Determination of free cyanide by distillation followed by colorimetry	E015
Soil	AR	Cyanide - Total	Determination of total cyanide by distillation followed by colorimetry	E015
Soil	D	Cyclohexane Extractable Matter (CEM)	Gravimetrically determined through extraction with cyclohexane	E011
Soil	AR	Diesel Range Organics (C10 - C24)	Determination of hexane/acetone extractable hydrocarbons by GC-FID	E004
Soil	AR	Electrical Conductivity	Determination of electrical conductivity by addition of saturated calcium sulphate followed by electrometric measurement	E022
Soil	AR	Electrical Conductivity	Determination of electrical conductivity by addition of water followed by electrometric measurement	E023
Soil	D	Elemental Sulphur	Determination of elemental sulphur by solvent extraction followed by GC-MS	E020
Soil	AR	EPH (C10 – C40)	Determination of acetone/hexane extractable hydrocarbons by GC-FID	E004
Soil	AR	EPH Product ID	Determination of acetone/hexane extractable hydrocarbons by GC-FID	E004
Soil	AR	EPH TEXAS (C6-C8, C8-C10, C10-C12, C12-C16, C16-C21, C21-C40)	Determination of acetone/hexane extractable hydrocarbons by GC-FID for C8 to C40. C6 to C8 by headspace GC-MS	E004
Soil	D	Fluoride - Water Soluble	Determination of Fluoride by extraction with water & analysed by ion chromatography	E009
Soil	D	FOC (Fraction Organic Carbon)	Determination of fraction of organic carbon by oxidising with potassium dichromate followed by titration with iron (II) sulphate	E010
Soil	D	Loss on Ignition @ 450oC	Determination of loss on ignition in soil by gravimetrically with the sample being ignited in a muffle furnace	E019
Soil	D	Magnesium - Water Soluble	Determination of water soluble magnesium by extraction with water followed by ICP-OES	E025
Soil	D	Metals	Determination of metals by aqua-regia digestion followed by ICP-OES	E002
Soil	AR	Mineral Oil (C10 - C40)	Determination of hexane/acetone extractable hydrocarbons by GC-FID fractionating with SPE cartridge	E004
Soil	AR	Moisture Content	Moisture content: determined gravimetrically	E003
Soil	D	Nitrate - Water Soluble (2:1)	Determination of nitrate by extraction with water & analysed by ion chromatography	E009
Soil	D	Organic Matter	Determination of organic matter by oxidising with potassium dichromate followed by titration with iron (II) sulphate	E010
Soil	AR	PAH - Speciated (EPA 16)	Determination of PAH compounds by extraction in acetone and hexane followed by GC-MS with the use of surrogate and internal standards	E005
Soil	AR	PCB - 7 Congeners	Determination of PCB by extraction with acetone and hexane followed by GC-MS	E008
Soil	D	Petroleum Ether Extract (PEE)	Gravimetrically determined through extraction with petroleum ether	E011
Soil	AR	pH	Determination of pH by addition of water followed by electrometric measurement	E007
Soil	AR	Phenols - Total (monohydric)	Determination of phenols by distillation followed by colorimetry	E021
Soil	D	Phosphate - Water Soluble (2:1)	Determination of phosphate by extraction with water & analysed by ion chromatography	E009
Soil	D	Sulphate (as SO4) - Total	Determination of total sulphate by extraction with 10% HCl followed by ICP-OES	E013
Soil	D	Sulphate (as SO4) - Water Soluble (2:1)	Determination of sulphate by extraction with water & analysed by ion chromatography	E009
Soil	D	Sulphate (as SO4) - Water Soluble (2:1)	Determination of water soluble sulphate by extraction with water followed by ICP-OES	E014
Soil	AR	Sulphide	Determination of sulphide by distillation followed by colorimetry	E018
Soil	D	Sulphur - Total	Determination of total sulphur by extraction with aqua-regia followed by ICP-OES	E024
Soil	AR	SVOC	Determination of semi-volatile organic compounds by extraction in acetone and hexane followed by GC-MS	E006
Soil	AR	Thiocyanate (as SCN)	Determination of thiocyanate by extraction in caustic soda followed by acidification followed by addition of ferric nitrate followed by colorimetry	E017
Soil	D	Toluene Extractable Matter (TEM)	Gravimetrically determined through extraction with toluene	E011
Soil	D	Total Organic Carbon (TOC)	Determination of organic matter by oxidising with potassium dichromate followed by titration with iron (II) sulphate	E010
Soil	AR	TPH CWG (ali: C5- C6, C6-C8, C8-C10, C10-C12, C12-C16, C16-C21, C21-C34, aro: C5-C7, C7-C8, C8-C10, C10-C12, C12-C16, C16-C21, C21-C35)	Determination of hexane/acetone extractable hydrocarbons by GC-FID fractionating with SPE cartridge for C8 to C35. C5 to C8 by headspace GC-MS	E004
Soil	AR	TPH LQM (ali: C5-C6, C6-C8, C8-C10, C10-C12, C12-C16, C16-C35, C35-C44, aro: C5-C7, C7-C8, C8-C10, C10-C12, C12-C16, C16-C21, C21-C35, C35-C44)	Determination of hexane/acetone extractable hydrocarbons by GC-FID fractionating with SPE cartridge for C8 to C44. C5 to C8 by headspace GC-MS	E004
Soil	AR	VOCs	Determination of volatile organic compounds by headspace GC-MS	E001
Soil	AR	VPH (C6-C8 & C8-C10)	Determination of hydrocarbons C6-C8 by headspace GC-MS & C8-C10 by GC-FID	E001


D Dried
AR As Received

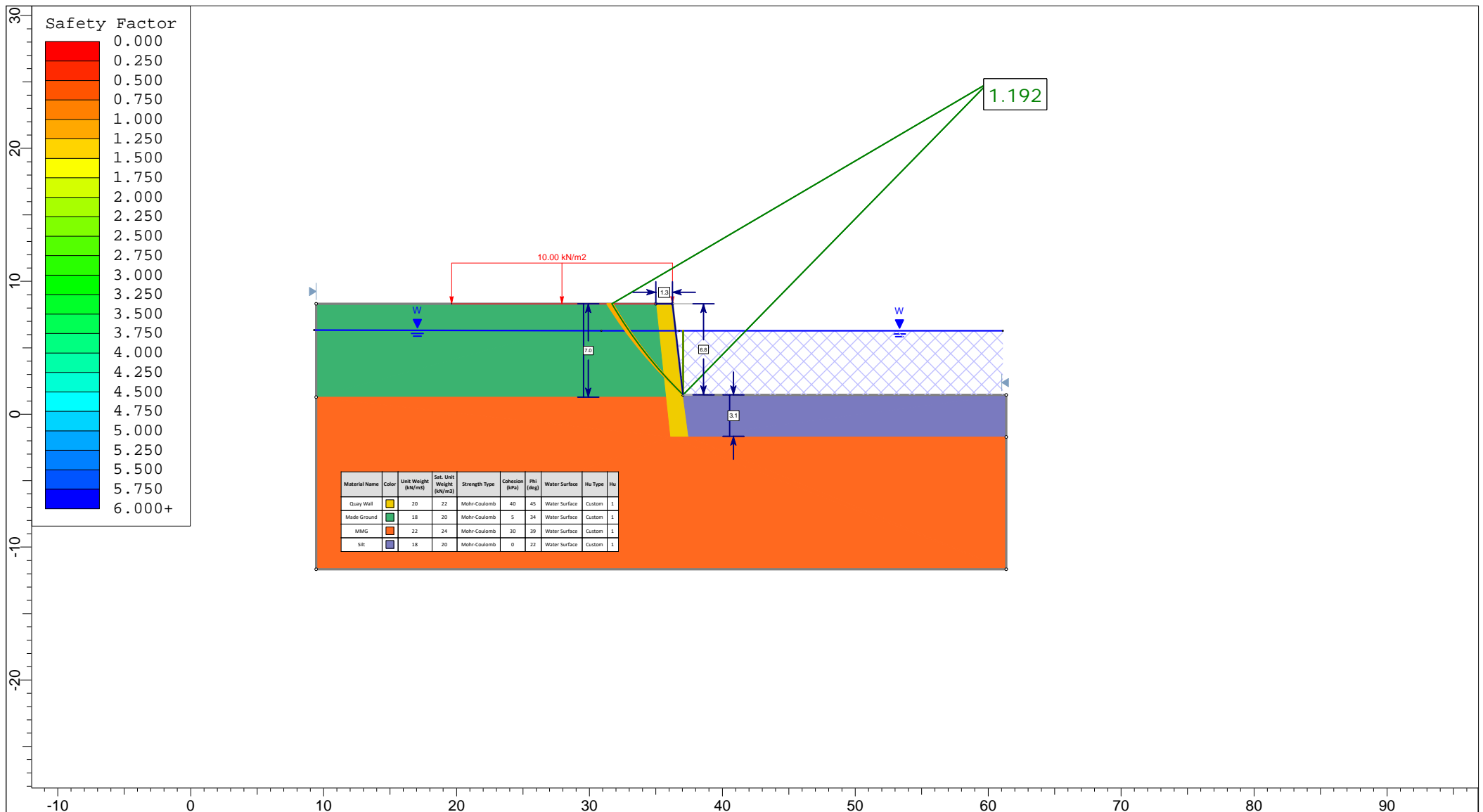
Appendix H


Stability Analysis Results

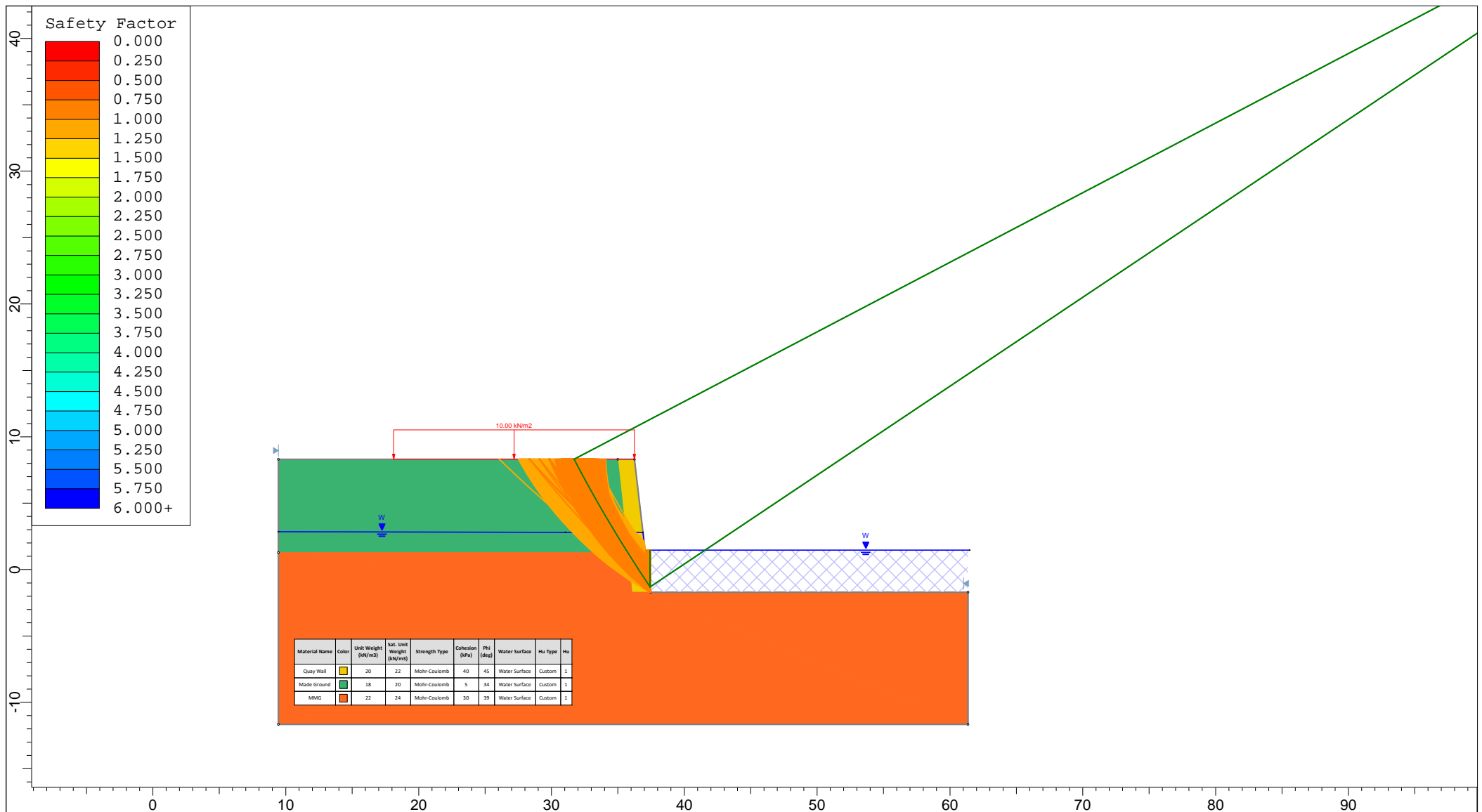


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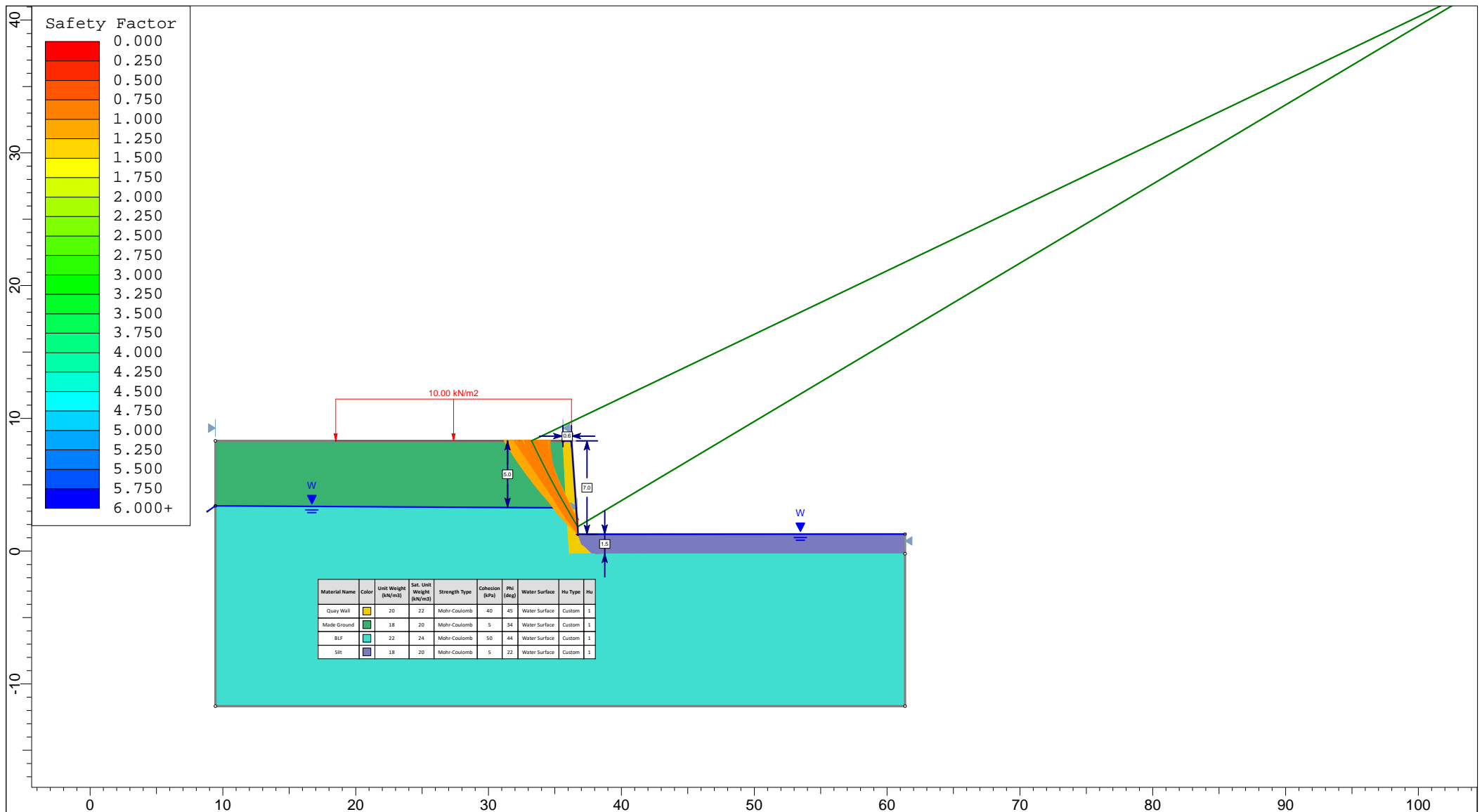
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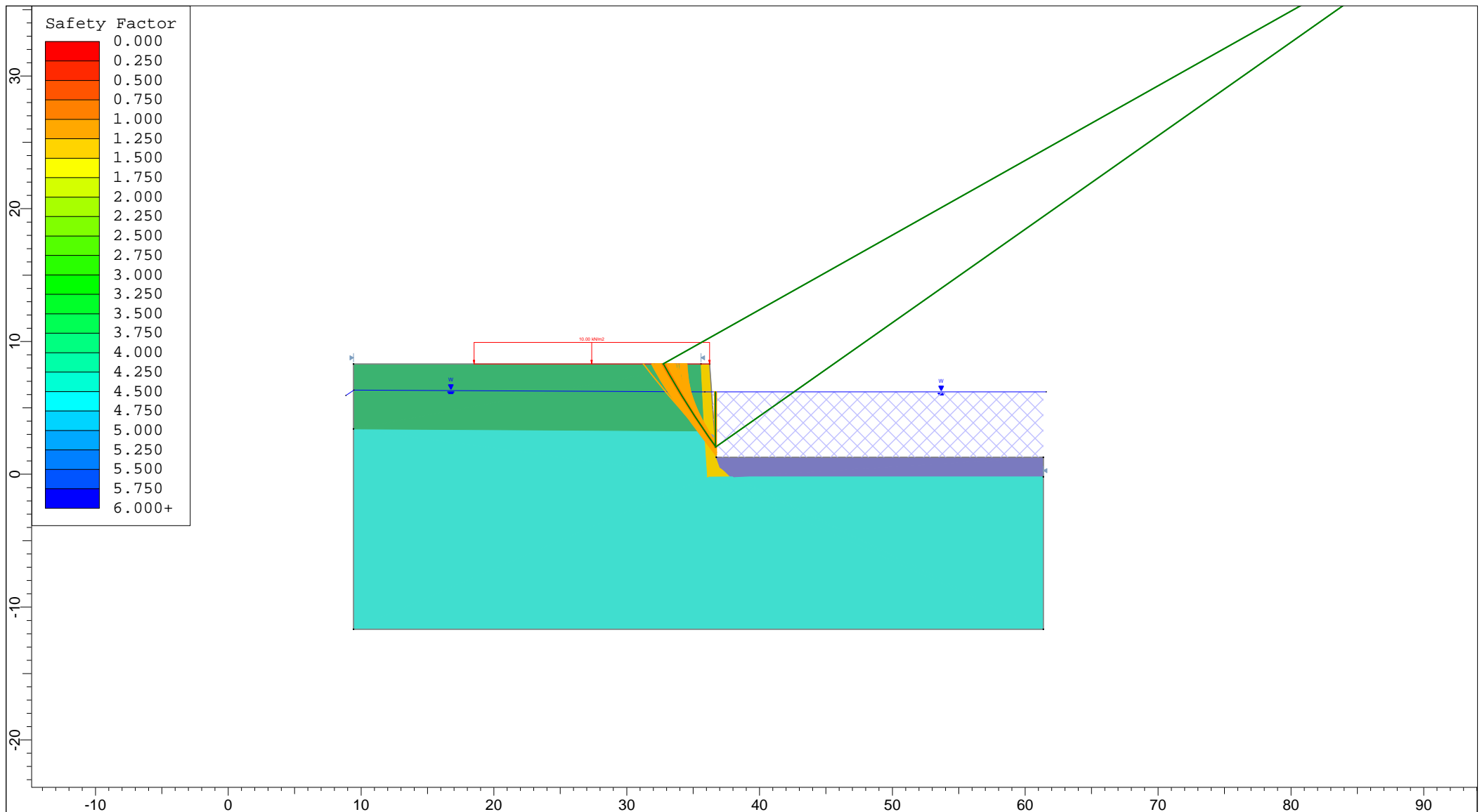
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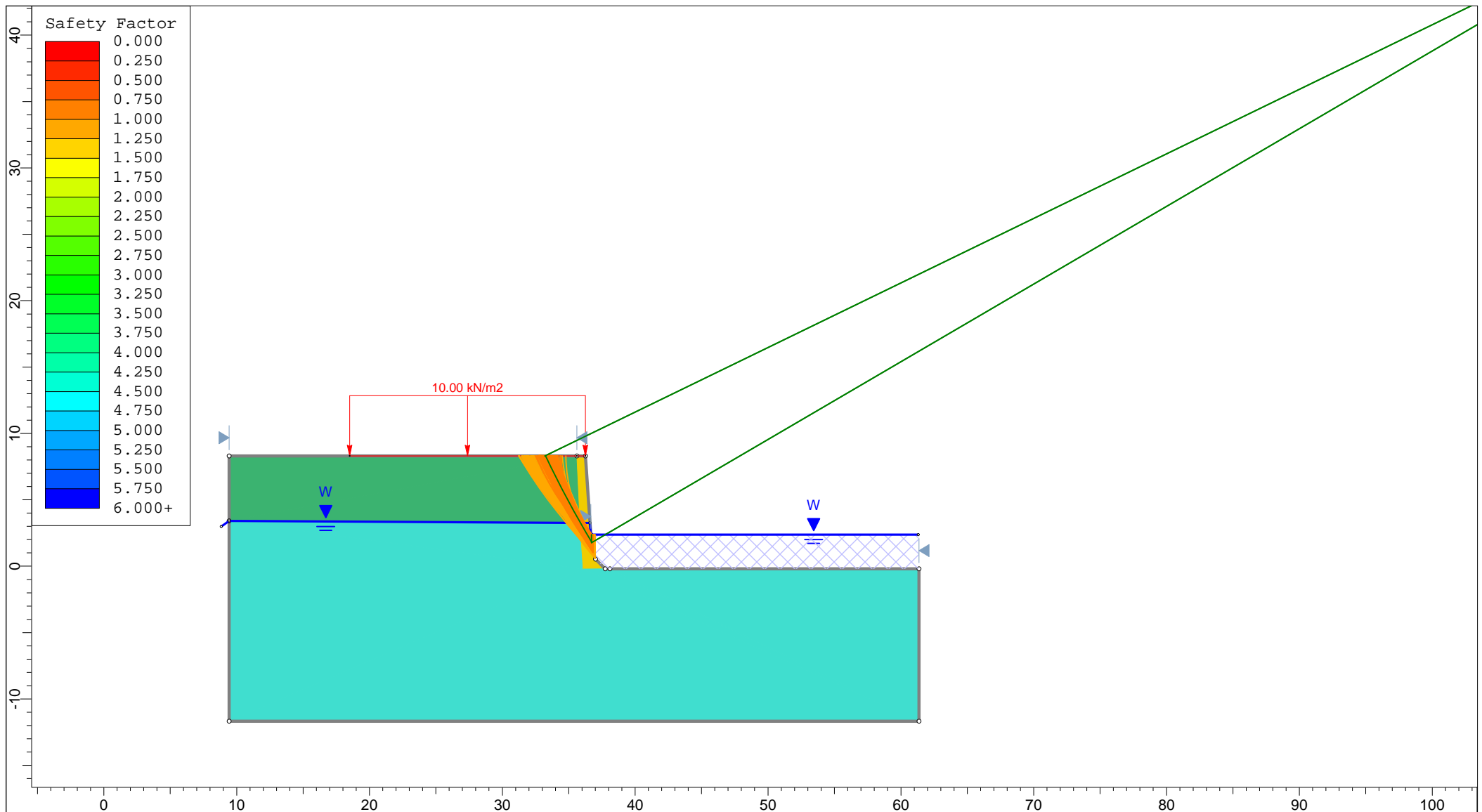
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	1:400		
	Date	File Name	
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SLIDEINTERPRET 8.020			



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 rocscience	Project		
	SLIDE - An Interactive Slope Stability Program		
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	Section 3 BH105 Dredged		
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